A

DISSERTATION REPORT
ON

# DESIGN AND ANALYSIS OF SPIRAL PHOTONIC CRYSTAL FIBER WITH CIRCULAR AND ELLIPTICAL AIR HOLES FOR FLATTENED DISPERSION AND BIREFRINGENCE PROPERTIES 

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## CERTIFICATE

This is to certify that the dissertation report entitled "DESIGN AND ANALYSIS OF SPIRAL PHOTONIC CRYSTAL FIBER WITH CIRCULAR AND ELLIPTICAL AIR HOLES FOR FLATTENED DISPERSION AND BIREFRINGENCE PROPERTIES" submitted by JULIE DEVI (2015PEC5306), in partial fulfilment of Degree Master of technology in Electronics and Communication Engineering during academic year 2016-2017. To best of my knowledge and belief that this work has not been submitted elsewhere for the award of any other degree.

The work carried out by her has been found satisfactory under my guidance and supervision in the department and is approved for submission.

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This Dissertation report on "DESIGN AND ANALYSIS OF SPIRAL LATTICE PHOTONIC CRYSTAL FIBER CIRCULAR AND ELLIPTICAL AIR HOLES FOR FLATTENED DISPERSION AND BIREFRINGENCE PROPERTIES" is carried out under the valuable guidance of supervisor Dr. Ritu Sharma (Assistant professor, ECE, MNITs, Jaipur).

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## List of Abbreviations

| PCF | Photonic Crystal fiber |
| :--- | :--- |
| FEM | Finite Element Method |
| PBGF | Photonic Fiber Bragg Grating |
| LFM | localized Function Method |
| SIF | Step Index Fiber |
| HC-PCF | Hollow Core Fiber |
| FDTD | Finite Difference Time Domain |
| TIR | Total Internal Reflection |
| FBG | Photonic Brag grating |
| PMF | Polarization maintaining fiber |
| DCF | Dispersion Compensation Fiber |


#### Abstract

In this thesis, spiral PCF with circular and elliptical air hole is designed and analysed for various optical properties. All layouts are simulated by Comsol 5.1 software. In this report, spiral type photonic crystal fiber (PCF) designed by varying diameter of air hole and arrangement of air hole in cladding region. Two types of layouts 1) circular air hole spiral PCF 2) elliptical air hole spiral PCF designed and reported in this thesis. In the first layout, the diameter of air hole is changed and all other parameters are kept constant. In this layout three different dimension configurations are considered with a) $\mathrm{d}=0.6 \mu \mathrm{~m} \mathrm{~b}$ ) $\mathrm{d}=0.8 \mu \mathrm{~m} \mathrm{c}) \mathrm{d}=1 \mu \mathrm{~m}$ of air holes. Low dispersion examined as compared to conventional PCF.

The second layout consists elliptical arrangement of air holes. This design is optimized for large flattened dispersion and high birefringence. Three configurations have been designed with three different dimensions. a) minor axis diameter $=0.55 \mu \mathrm{~m}$, major axis diameter $=0.45 \mu \mathrm{~m}$ b) minor axis diameter $=0.62 \mu \mathrm{~m}$, major axis diameter $=0.40 \mu \mathrm{~m}$ c) ellipticity ratio vary from first to last ring. These two designs have been compared with each other and examined for different propagation property of light waves such as dispersion, effective area, effective refractive index, and birefringence. these layouts, silica is used as a substrate material having refractive index 1.45. It has been analysed that as we change the geometry of PCF all properties get changes. It has been observed that as the diameter of the air hole is changed, dispersion changes with wavelength and very high birefringence is obtained for elliptical air hole arrangement as compared to circular air hole PCF. Thus, the optimized design can be used as low flattened dispersion PCF for sensing application.


## INTRODUCTION

### 1.1 Introduction

Since the introduction of conventional step index fibers, optical fibers have evolved into many forms in the 70s and later single material fiber where effective cladding structures determined the propagation of light. The principle objective was the transportation of light from one point to another whether by step index confinement or by band-gap confinement such as in Bragg fiber. We can use optical fiber in many applications like transporting high speed data, bio sensors Etc. the optical fiber can also use in Gas sensing application, strain or pressure measurement in bridges and highpower amplifier. Photonic Crystal Fibers (PCF) is a variant of the micro structured fibers with greater control of guiding properties. Such a vital Photonic Crystal fiber have large application area in nonlinear devices and high power optical fiber amplifier.

### 1.2 History of PCF

Optical fibers were discovered in the 1970s and are now the backbone of opticalcommunication systems due to a large amount of information they can handle. Particularly designed optical fibers are also used for many optical applications, including sensors, medicine, illumination and much more. Standard step-index optical fibers guide light through total internal reflection, which occurs only if the core has a larger refractive index than the outer cladding. The optical signal propagates in the core is completely reflected at the interface core/cladding and is, therefore guided in the core. First fiber is fabricated by Russell consist hexagonal lattice in silica fiber. These novel periodic structures were called photonic crystals. Only light with certain wave vectors can propagate in the structure If a defect or periodic structure is introduced in the is in the structure, the wavelengths forbidden in the periodic structure are now allowed to "stay" in the defect as the photonic crystal running along the air hole prevents them from "escaping". The refractive index is not required to be higher than that of the periodic
material. By using this idea light can be trapped inside a hollow core (defect). Therefore, light can even be guided in the air.[8]

### 1.3 Theory of PCF

In the last decade, photonic crystal fibers have been under rigorous study and due to the development of PCF and unique application, attracted huge research interest. PCF is a fiber which contains its different optical properties from particularly varying the design and arrangement of air holes in fiber which run through the length of the fiber, not from different glass composition. The simplest type of PCF has triangular lattice. Photonic crystal fiber is categorized into two types of mechanism 1) Photonic band Gap 2) Total Internal reflection


Fig 2.1 geometry of hexagonal PCF

### 1.3.1 Advantage of Photonic Crystal Fiber

$>$ Better light confinement than conventional fibers
$>$ Low dispersion
> Very low attenuation (holey fiber)
> More flexible than conventional fibers
$>$ Many core fiber

### 1.3.2 Basics equations

Propagation of light in PCFs is described by Maxwell's equations. For no free charge or current, the following equations become applicable

$$
\begin{gather*}
\nabla . D=0 \\
\nabla \times H=\frac{\partial D}{\partial t} \\
\nabla . B=0 \\
\nabla \times E=-\frac{\partial B}{\partial t}  \tag{2.1}\\
\varepsilon(\mathrm{r}, \omega)=\varepsilon(\mathrm{r}) \in R \\
\mathrm{D}(\mathrm{r})=\varepsilon(r) \times \varepsilon o \times E(r) \\
\mathrm{B}=\mu o \times H \tag{2.2}
\end{gather*}
$$

(a)

Inserting equation b into a

$$
\begin{align*}
& \nabla . \varepsilon(r) \times \epsilon o \times E(r, t)=0 \\
& \nabla \times H(r, t)=\varepsilon(r) \times \varepsilon o \times \frac{\partial E(r, t)}{\partial t} \\
& \nabla . \mu o . H(r, t)=0  \tag{2.3}\\
& \nabla \times E(r, t)=-\mu o \cdot \frac{\partial H(r, t)}{\partial t}
\end{align*}
$$

Since Maxwell's equations are linear we can separate out the time dependence by expanding into
a set of harmonic modes

$$
\begin{aligned}
& H(r, t)=H(r) \cdot e^{j \omega t} \\
& E(r, t)=E(r) \cdot e^{j \omega t}
\end{aligned}
$$

To obtain coupled equations we need the following ones

$$
\begin{gather*}
\nabla \cdot \varepsilon(r) \cdot E(r)=0  \tag{2.4}\\
\nabla \times H(r, t)=j \omega \varepsilon(r) \varepsilon o E(r) \\
\nabla \cdot H(r)=0 \\
\nabla \times E(r)=j \omega \cdot \mu o \cdot H(r) \tag{2.5}
\end{gather*}
$$

### 1.4 Guiding mechanism in PCF <br> 1.4.1 Total internal reflection

In solid core PCF light, is comes from high refractive index core to lower refractive index cladding. Light is kept in the core by total internal reflection in photonic crystal fiber. In PCF, When the angle of incident is greater is greater than the critical angle, total internal reflection takes place in solid core fiber.
1.4.2 Photonic bandgap in photonic crystal fiber defects is created by introducing air hole in fiber and the photonic band gap is created.in this case light guidance mechanism is like electron conduction mechanism in solid-state physics. Photonic band gap structure offer opportunity to design new optical property in existing fiber. Due to the presence of air hole, light is confined in the core region and these modes guided along the defect through the fiber.

### 1.5 Properties of PCF

### 1.5.1 Confinement loss

The losses in PCFs occur for many reasons, such as Rayleigh scattering loss, intrinsic material absorption loss, macro and micro binding loss, and so on. Fabrication related losses can be reduced by carefully optimizing the fabrication process. The Periodic arrangement of air holes in PCF causes a decrease in optical confinement, is called Confinement loss. PCF is made by single material and so guided mode is leaky. The region of loss is that the refractive index of the core is same the refractive index of the cladding. Confinement loss depends on the structure and arrangement of air holes in PCF. We can alter the value of loss by changes the geometry of fiber. For analyzing the
confinement loss, PML layer is applied to PCF. With the help of PML layer, we find the value of the imaginary refractive index and find the confinement loss.

$$
\begin{equation*}
\text { Confinement loss }=8.686 \times 10^{6} \times \mathrm{ko} \times \mathrm{im}\left(\mathrm{n}_{\mathrm{eff}}\right) \tag{dB/m}
\end{equation*}
$$

### 1.5.2 Normalized frequency

The $V$ parameter (normalized frequency) is commonly used in the design of conventional SIFs and is given by

$$
V=\frac{2 \pi \mathrm{a}}{\lambda} \times \sqrt{\mathrm{n}_{\mathrm{co}}^{2}}-\mathrm{n}_{\mathrm{cl}}^{2}
$$

To finding the V parameter for PCF, its different nature is considered. V parameter of PCF given as

$$
V_{\mathrm{PCF}}=\frac{2 \pi \mathrm{a}}{\mathrm{w}} \times \sqrt{\mathrm{n}_{\mathrm{FM}}^{2}}(\mathrm{w})-\mathrm{n}_{\mathrm{FSM}}^{2}(\mathrm{w})
$$

Where $n_{F M}(w)$ is wavelength dependent refractive index of fundamental mode and $n_{F S M}^{2}(\mathrm{w})$ is fundamental space filling factor. For single mode fiber $V_{\text {PCF }}$ should be equal to $\pi$.

### 1.5.3 Effective modal area

The effective mode area $A_{e f f}$, is computed using transverse electric or magnetic field vector of the whole cross-sectional area of the fiber. The effective area of the of the fiber core $A_{\text {eff }}$ is defined as [2]

$$
A_{e f f}=\frac{\left(\int \mid E_{t \mid}^{2} d x d y\right)^{2}}{\int \mid E_{t \mid}^{4} d x d y}
$$

Or

$$
A_{e f f}=\frac{\left(\iint \mid H_{t \mid}^{2} d x d y\right)^{2}}{\iint \mid H_{t \mid}^{4} d x d y}
$$

where $E_{t}$ and $H_{t}$ is the transverse electric field vector and magnetic field vector respectively and the integration is done through the whole cross-sectional area of the fiber.

### 1.5.4 Chromatic dispersion

Effective refractive index of mode profile depends on wavelength. Relation between wavelength and refractive index is given by equation below

$$
\mathrm{v}=\frac{c}{n}
$$

All optical source used for optical transmission emit light, in the band of spectral width $\Delta \lambda$, distributed around $\lambda$.so individual frequency component experienced different velocity so different frequency component travel with different speed and pulse get dispersed. The speed at which light travel through fiber rely on its wavelength and design of fiber thus some wavelength of band of which the pulse is embraced may be delayed compared with other, leading to pulse spreading with time after traversing a significant length of fiber called chromatic(Total) dispersion. Total dispersion is the sum of two form of dispersion (1) material dispersion (2) waveguide dispersion. The chromatic dispersion D of a PCF is calculated from given formula [18-20]

$$
\mathrm{D}=-\frac{\lambda}{\mathrm{C}} \times \frac{\mathrm{d}_{\text {neff }}^{2}}{\mathrm{~d} \lambda^{2}}
$$

where c is the velocity of light in a vacuum $\mathrm{n}_{\text {eff }}$ is effective refractive index of PCF.

### 1.5.4.1 Material dispersion

The material refractive index depends on the value of wavelength. Material dispersion is calculated by a sellmeier equation which gives the relation between refractive index and wavelength. Usual form of equation is given as [22]

$$
\mathrm{n}^{2}(\mathrm{w})=1+\frac{\mathrm{B}_{1} \mathrm{w}^{2}}{\mathrm{w}^{2}-\mathrm{C}_{1}}+\frac{\mathrm{B}_{2} \mathrm{w}^{2}}{\mathrm{w}^{2}-\mathrm{C}_{2}}+\frac{\mathrm{B}_{3} \mathrm{w}^{2}}{\mathrm{w}^{2}-\mathrm{C}_{3}}
$$

where n is refractive index of material and w is operating wavelength. Coefficient $\mathrm{B}_{1,2,3}$ and $C_{1,2,3}$ is experimentally examine. The coefficient of the sellmeier equation is different for different material.

### 1.5.4.2 Waveguide dispersion

Waveguide dispersion depends on the fiber refractive index profile. Waveguide dispersion is significant for the fiber having small effective area. Altering the refractive index profile will alter the waveguide dispersion.

$$
\mathrm{D}=\frac{\lambda}{\mathrm{c}} \frac{\mathrm{~d}^{2} \mathrm{n}}{\mathrm{~d} \lambda^{2}}
$$

### 1.5.5 Modal birefringence

Effective index profile sometimes depends on the polarization and propagation direction of optical signal. So the refractive index of the two fundamental modes ( $x$ and $y$ mode) will not be same. Birefringence is the difference of effective refractive index between these two-fundamental modes. Birefringence can be calculated using the equation [9]

$$
\text { Birefringence }=\left[\mathrm{n}_{\mathrm{eff}}(\mathrm{X} \text { mode })-\mathrm{n}_{\mathrm{eff}}(\mathrm{Y} \text { mode })\right]
$$

### 1.5.6 Non-linearity

The nonlinear effect in optical fiber occurs due to intensity dependence of refractive index in medium or different scattering phenomenon. Nonlinearity is a most important phenomenon in optical fiber communication and used in various applications such as four-wave mixing, Supercontinuum generation and self-phase modulation. Nonlinearity depends on the type of material and design of fiber. Nonlinearity is calculated with the help of nonlinear coefficient that is different to different materials. [12]

$$
\gamma=\frac{2 \pi}{\lambda} \times \frac{\mathrm{n}_{2}}{\mathrm{~A}_{\mathrm{eff}}}
$$

where $\mathrm{n}_{2}$ is nonlinear coefficient

### 1.6 Applications of PCF

### 1.6.1 Dispersion compensation Fiber

DCF is a simple and developed technology used in optical communication system. Commercially available DCF can compensate the dispersion of all transmission fiber even for high bit rate and long distance. The newest development in DCF reduced losses and length of optical fiber. This fiber can also be used as dispersion shifted fiber. [33]

### 1.6.2 Polarization maintaining PCF

Optical fiber always shows some amount of birefringence even if PCF has a circular design because in fabrication process there is always some stress or pressure which breaks the symmetry of fiber because of this polarization of light propagating in the fiber regularly changes in an uncontrolled manner. To remove this problem PMF is used. PMF has a high value of birefringence. The polarization of light launched into the fiber is aligned with one of the birefringence axes and polarization is maintained even if the fiber is bent. Due to strong birefringence, the propagation constant of two polarization modes is different so the relative phase of such copropagating modes rapidly drift away so any disturbance in giber does not affect large enough on polarization direction. [32]

### 1.6.3 Hollow core fiber

Hollow core fibers light is guided by using a photonic bandgap structure in place of a traditional total internal reflection. Since most of the optical power propagates through the core region, not cladding region, these fibers are particularly unaffected by nonlinear optical effects. Hollow core fibers can offer other advantages like extremely low loss bends, extreme dispersion values and the ability to modify the core material properties by exchange air for some other gas and HC-PCF can be used as microcell.

### 1.6.4 Fiber laser amplifier

Fiber amplifiers are one of the key components of modern telecommunication. Also, fiber lasers are starting to be more and more important in medicine, spectroscopy, and industry. Compared to conventional solid-state lasers, the great advantage of fiber lasers is their outstanding heat dissipation capability. The fiber laser is insusceptible to thermal
lensing and all other temperature properties. The one most important advantage of fiber laser amplifier than a conventional laser is the quality of stream of light which is close to the diffraction limit.

## CHAPTER 2

## ANALYSIS METHOD

### 2.1 Methodology

In general, three methods are utilized to analyze the structure and the properties of photonic crystal fibers. They are
$>$ Effective refractive Index Approach
$>$ Basis-Function Expansion Approach
$>$ Numerical Approach

### 2.1.1 Effective Index approach

The first approach developed for PCFs was the effective index approach based on a very simple scalar model using an effective cladding index. In this approach propagation of light is through slab like PCF is commonly describe in terms of refractive indices, we can replace 3D structure by an effective 2D refractive index profile .first, an effective index for the periodically repeated hole-in-silica structure is evaluated and then the microstructured cladding region is replaced by a uniform medium with a properly chosen effective index, resulting in an equivalent step index fiber (SIF) consisting of a core and a cladding region. Using this simple model and the well-established fiber theory, we can obtain a qualitative information about PCFs with perfect hexagonal symmetry. The core is pure silica, but the effective cladding index is determined by using the propagation constant of the lowest-order fundamental mode propagating in the periodically repeated hole-in-silica structure without any defects. The propagating modes in such an infinite cladding material are called space filling modes, the propagation constants of which are strongly dependent on the operating wavelength $\lambda$. The propagation constants of the space-filling modes are usually calculated by solving an approximate scalar-wave equation within a unit cell centered on one of the air holes. By reflection symmetry, the Neumann condition is enforced on each cell edge, namely, the normal derivative of the cladding mode field to the edge must be zero.

### 2.1.2 Basic Function Expansion approach

Although the effective index approach can provide good qualitative information about PCFs, this approach is unable to accurately predict modal properties such as dispersion or birefringence. These quantities depend critically on PCF geometries. An early fullvector model for PCFs has been based on a modal decomposition technique using various basis functions such as sinusoidal functions, Hermite-Gaussian functions and cylindrical functions. The PWE has been effectively applied not only to index guiding PCFs but also to PBGFs. PWE involves defining the supercell over a restricted region and using periodic boundary conditions to extend the structure spatially, and therefore, the applicability to PCFs that do not need to be periodic is somewhat restricted. An alternative approach is a localized-function method (LFM). As the guided modes in PCFs are localized in the defect core region, their modal fields are well described using localized Hermite-Gaussian functions. The LFM takes advantage of mode localization, and thus, a modest number of functions are required to accurately model the guided modes, resulting in less computational efforts, compared with the PWE.

### 2.1.3 Numerical approach

Although the basis-function expansion approach can accurately predict the modal properties such as dispersion and birefringence, it is difficult to apply it to more complicated fibers with noncircular air holes and/or longitudinally varying structures. Recently, published models utilize other direct numerical analysis techniques such as BPM, FDM, FDTD, BEM, and FEM. In the FEM, instead of solving the wave equation, the corresponding functional to which a variational method is applied is set up, where the fiber cross section is divided into the so-called elements, an equivalent discretized model for each element is constructed, and then all the element contributions to the whole fiber cross section are assembled.

### 2.2 Full Vectored Finite Element Method

$>$ A finite element optical mode solver is the most popular method to thoroughly analyze photonic crystal fibers. The finite element method is a numerical approximation process used for the solution of boundary and initial value problems for differential equations
$>$ The FEM produces approximate solutions by writing them as linear combinations of simple basis functions and test functions equal to the basic functions and introducing these into the variational formulation of the problem
$>$ The final FEM equations that must be solved are systems of linear algebraic equations
$>$ COMSOL is modern software embedding the FEM with a cleverly designed user interface designed to increase the applicability and ease of use of mathematical modeling methods
There is different matched layer condition in finite element method.
2.2.1 Perfect Magnetic conductor: - This boundary condition can be expressed as

$$
\begin{gathered}
n . D=0 \\
n \times H=0
\end{gathered}
$$

According to this condition, tangential components of H and normal components of D is continuous across any interface
2.2.2 Perfect Electric conductor This boundary condition can be expressed as

$$
\begin{aligned}
n . B & =0 \\
n \times E & =0
\end{aligned}
$$

Here, n is the unit normal vector to the boundary. According to this condition, tangential components of E and normal components of B is continuous across any interface.

### 2.3 Comsol Multiphysics

COMSOL MULTIPHYSICS software is used to simulate different properties of PCF which is based on finite element method. COMSOL software (5.1) is used for the numerical answers \& graphs of different parameters of spiral PCF and the results are reported in this thesis.

### 2.3.1 Design of PCF using COMSOL

$>$ Open software COMSOL 5.1. A window named Model Wizard will be opened
> Then following steps are followed: optics Module>Wave optics>Electromagnetic, frequency domain Waves>Mode analysis
$>$ The software is opened with working window.
To design the structure of a PCF first set it at appropriate modal analysis, then draw the structure of PCF and give input for geometrical properties, initialize mesh and then solve the structure. The procedure for this work is given bellow

### 2.3.1.1Setting appropriate parameter and study

$>$ We Select Physics in the Physics menu to open the Application Mode Properties dialog box.
$>$ We select the correct study using Add study dialog box
$>$ We select the appropriate parameter for our geometry and define all the parameter in setting window of the parameter.

### 2.3.1.2 Geometry Modeling

$>$ On geometry, toolbar click primitive and choose circle
$>$ In setting window of circle locate size and shape
$>$ We start by drawing a circle with the radius and the center at desired values with right click in geometry icon.
$>$ In geometry tool bar click transforms and select rotate.
$>$ Click the build all object button.

### 2.3.1.3 Material setting

$>$ After making the geometry of PCF we add material in our geometry.
> First, click on material toolbar and select blank material and write the refractive index of material in material setting window
$>$ Select domain

### 2.3.1.4 Mesh setting

$>$ In modal builder window $>$ component 1 click mesh 1
$>$ In setting window for mesh choose physics controlled Mesh
$>$ From element size list select between fine to extra coarser
> Click on build all button

### 2.3.1.5 Study Setting

$>$ In modal builder window under study 1 click mode analysis.
$>$ In the setting window for mode, analysis locates the study setting window.
$>$ In the search for mode around a text field type refractive index of the core.
$>$ In the search for frequency around text field type frequency.
$>$ On the home, toolbar clicks compute.

### 2.3.1.6 Post processing

$>$ In modal builder window under result click 1D plot group.
$>$ Under 1D plot group select line graph.
$>$ Plot line graph between wavelength and $n_{e f f}$.
$>$ Extract spreadsheet from comsol to excel.

## CHAPTER 3

## LITERATURE SURVEY

Md Asiful Islam and M Shah Alam proposed a structure of spiral PCF. This PCF can be used to compensate the dispersion properties and used for supercontinuum generation. The structure contains the air holes in silica material. there is N circular air hole in each arm and diameter of each air hole is increased progressively. The angular displacement of each arm is $\theta$ than by previous one. the proposed structure contains an elliptical air hole at the center of air core This design is simulated by comsol Multiphysics which is based on full vector finite element method. The design of PCF shows the dispersion of 293.5 and $-393 \mathrm{ps} / \mathrm{nm} \mathrm{km}$. another exceptional feature of this design is their high birefringence of 0.0278 .

Agrawal, A., Kejalakshmy, N., Rahman, B.M.A. and Grattan, K.T.V. (2009) [2] the proposed spiral PCF fiber design in the SF57 is presented with high nonlinearity with low and flattened dispersion. The design of PCF is inspired by nature. Each arm of PCF contains air holes with constant radius $r$ and angular displacement $\theta$. A full vector finite element method is used to simulate the design. ES-PCF design in SF57 has been presented that have high nonlinearity of $2150 / \mathrm{W} . \mathrm{km}$ at 1550 nm and also the PCF optimized for low dispersion of $0.8 \mathrm{Ps} / \mathrm{nm} . \mathrm{km}$. it combines the advantage of better dispersion control with the smaller effective area and high nonlinearity.
M. Samiul Habib, M. Selim Habib, M. Imran Hasan, S.M.A Razzak (2013) [3], this paper presents a soft glass spiral photonic crystal fiber for tune two zero dispersion wavelength in the visible and near infrared region. The design contains six circular rings and eight spiral arm, each air hole of the first ring is the starting point of a spiral arm. The distance of second air ole in the spiral arm from the center is $\mathrm{r}_{\mathrm{b} 1}=\mathrm{r}_{b 0}+0.8\left(2 \times \mathrm{r}_{\mathrm{a}}\right)$ with an angular shift $\theta_{1}=\frac{360}{2 \times \mathrm{N}}$ where N is the number of spiral arms. To produce high birefringence, an artificial defect is introduced in the core region. The designed fiber has two ZDW at 700 nm and 1050 nm with very large nonlinearity of $7326 / \mathrm{W}$. Km at 700 nm and $3919 / \mathrm{W}$. Km at 1050 nm . The designed PCF offer birefringence of 0.1 at $1.8 \mu \mathrm{~m}$.
S. Revathi*, Srinivasa Inabathini, Ram Sandeep (2015) [4] This paper present a soft glass spiral photonic crystal fiber with a circular air hole for achieving high birefringence, large nonlinearity, and large negative dispersion. For achieving high birefringence, the defect is introduced in the core region. The structure is designed using the comsol 3.5 it is based on finite element method, an accurate numerical method used to find the solution of boundary problems. The structure contains 8 spiral arms and each arm contains five circular air hole. An elliptical air hole introduced in the center of core with semi major axis a and semi minor axis $b$. this fiber can be used as polarization maintaining fiber which has more control on polarization. This fiber optimized for high birefringence of $2.96 \times 10^{-2}$ at $1.55 \mu \mathrm{~m}$ and high nonlinearity of $5828 / \mathrm{W} . \mathrm{Km}$.this fiber give negative dispersion $-1546.6 \mathrm{ps} / \mathrm{nm}$. km at 850 nm .
S. Revathi*, Srinivasa Inabathini and Rizwan Ali Saifudeen (2014) [5] the proposed structure is designed with elliptical air hole using comsol. The structure is designed with chalcogenide glass. This structure is optimized for different ellipticity ratio of the air hole. The structure contains seven spiral arms and each arm contains five elliptical air holes. The angular displacement between two adjacent elliptical air hole is $\frac{180}{\mathrm{~N}}$ where N is the number of air holes in a ring. The effect of ellipticity ratio on the various property of fiber is observed. The advantage of spiral structure is low effective area and high nonlinearity. By obtaining result from simulation, we get high birefringence of order $10^{-2}$ which is larger than conventional PCF. Fiber offers high birefringence of 0.0256 at $1.55 \mu \mathrm{~m}$ and gets negative dispersion of -1136.69 at $.85 \mu \mathrm{~m}$. We can use this fiber in the nonlinear application.

Varshali Sharma, Ritu Sharma (2016) [6] the proposed design of PCF with elliptical and circular air hole is analysed for high birefringence and large flattened dispersion. There are five rings, inner three rings have elliptical air hole and outer two rings have circular air holes. These layouts are designed and analysed and also compare with layout having only circular air holes arrangement. From the analysis, we observed flattened dispersion over a large range from 1.2 to $1.8 \mu$ m.the proposed design also give high birefringence value which can be used in various sensing application.

Philip St.J. Russell (2006) [7] Photonic crystal fiber with a periodic transverse microstructure have been in practical since 1996. It is now possible to manufacture PCF of a scale 10 nm on a scale of 1 um scale, which allows exceptional control on optical properties like dispersion, effective area, birefringence and nonlinearity of optical fiber. The novel idea for developing PCFs was the creation of a new design dielectric waveguide, one that guides light by means of a two-dimensional (2-D) PBG. the idea was to trap the light in two dimensional PCF by using air holes array.

Theis P. Hansen, Jes Broeng, Stig E. B. Libori, Erik Knudsen, Anders Bjarklev, Jacob Riis Jensen, and Harald Simonsen (2001) [9], photonic crystal fiber offers new possibilities of highly birefringence fiber due to large index difference between core and cladding region compared to conventional fiber. The proposed design consists triangular lattice of air holes with a pitch of $4.5 \mu \mathrm{~m}$. the core is made by removing two air holes. The fiber was found to exhibit the highest birefringence of $6.9 \times 10^{-4}$ at frequency $1.05 \mu \mathrm{~m}$. by optimizing the design of PCF, we get high birefringence at $1.55 \mu \mathrm{~m}$ for pitch ratio $1.7 \mu \mathrm{~m}$.
Md. Ibadul Islam, Kawsar Ahmed, Sayed Asaduzzaman, Bikash Kumar Paul a, Touhid Bhuiyan, Shuvo Sen, Md. Shadidul Islam, Sawrab Chowdhury (2017) [10], proposed structure consists air holes that are arranged in a hexagonal design of pitch $\Lambda$. The refractive index of the silica regions is 1.4445 . The holes are characterized by the area and ellipticity ratio $\frac{a}{b}$, where a and b are the diameter of the major and minor axes, respectively. Geometry of PCF is simulated for different ellipticity ratio and hole area is less than $0.4 \mu$ m.it has been observed from the result that on the holes area. whereas for larger holes and ellipticities, the core itself has an elongated elliptical shape. for small hole area and small ellipticity, birefringence depends only on the ellipticity and not on area.

Jianfei Liao, Junqiang Sun, Mingdi Du, and Yi Qin (2014) [11], the structure consists spiral photonic crystal fiber that is used as a sensor. This design can be used to sense the colorless gas and air pollution by metering gas condensate elements. The proposed structure simulated by finite element method. Design consist of a cluster of circular air holes in core region which are formed into porous shape and cladding is formed in a
spiral shape. The proposed structure gives high sensitivity and high birefringence for the wavelength range of $1 \mu \mathrm{~m}$ to $1.8 \mu \mathrm{~m}$. we get high birefringence of $7.23 \times 10^{-3}$ at $1.33 \mu \mathrm{~m}$. so proposed spiral PCF ensure major change in colorless and toxic gas detection.

Jianfei Liao, Tianye Huang, Zuzhou Xiong, Fangguang Kuang, Yingmao Xie (2017) [12] proposed design has been analysed for large flattened dispersion and high nonlinearity coefficient. Design consist slotted core region surrounded by the three rings of air hole in the spiral lattice. The optical properties of this fiber designed has been analysed for the wavelength range from 1.4 to $1.7 \mu \mathrm{~m}$. Simulation results show that the nonlinear coefficients as high as $224.36 \mathrm{~W}^{-1} \mathrm{~m}^{-1}$ and $226.39 \mathrm{~W}^{-1} \mathrm{~m}^{-1}$ respectively. Chromatic dispersion $(-5.64,2.62)$ for wavelength range 1.4 to $1.7 \mu \mathrm{~m}$.
Md. Ibadul Islam1, Maksuda Khatun1, Shuvo sen1, Kawsar Ahmed1 and Sayed Asaduzzaman (2016) [13] author proposed a design of spiral photonic crystal fiber having an elliptical slot in core region for purpose of controlling dispersion and birefringence property of PCF. Elliptical slot in the core region is made of SF57 (soft glass). fiber cladding consists of spiral lattice on fused silica having refractive index 1.45. the diameter of air hole in each arm is increase respectively. Here SF57 is used for two regions 1) SF57 has high nonlinearity.2) it enhances the confinement of light in high index SF57 area.in addition of this SF57 also alter the chromatic dispersion and destroy the symmetry of fiber and increase birefringence.by examining the design, the result shows birefringence of 0.0341 at $1.55 \mu$ m.dispersion at 1.55 is $-491.16 \mathrm{ps} / \mathrm{nm}-\mathrm{km}$.

Jianfei Liao Yingmao Xie Xinghua Wang Dongbo Li Tianye Huang(2017) [14], the proposed design of spiral PCF has been used in gas sensing application. Inner core region consists hexagonal lattice and shape of air holes is elliptical. Outer cladding region having spiral lattice. In fiber design, there is 10 spiral arms and each arm has 9 circular air holes. It has been observed from a simulation that relative sensitivity is $42.27 \%$ and due to the presence of hexagonal lattice in the core region, we observe high birefringence of order ( 0.01727 ) at $1.33 \mu \mathrm{~m}$ wavelength range.

Arti Agrawal, Y. O. Azabi and B. M. A. Rahman (2013) [15] the proposed structure contains slotted silicon PCF with ultra-high birefringence, nonlinearity, and ultrahigh flattened dispersion. Cladding consists of a triangular lattice of air holes of diameter D and pitch $\Lambda . \mathrm{in}$ addition of this a design consists elliptical silicon nichrome rod, is situated in the center of the core that breaks the symmetry of design and increases birefringence of fiber. Simulation result shows that by introducing silicon nichrome rod birefringence of order 0.0736 at $1.55 \mu \mathrm{~m}$ is achieved. Low dispersion of $.49 \mathrm{ps} / \mathrm{nm}-\mathrm{km}$ is achieved at 180 nm . The designed PCF can be used as power efficient optical application.

Ritu Sharma, Vijay Janyani, S. K. Bhatnagar (2011) [16], index core two-dimensional photonic crystal fiber has been proposed in this paper modal analysis is done by FDTD for TE and TM mode. The PCF consist three rings of elliptical air and compare with circular air hole design.by observing the result of simulating designs we analyse that elliptical air hole design gives lower dispersion as compared to circular air hole design.

Rui Hao, Guifang Sun (2015) [17], An elliptical spiral soft glass PCF has been designed and analysed for high birefringence. The geometry is inspired by nature, such as galaxies, distribution of sunflower, shells of snails etc. PCF consist 12 circular air hole and spiral lattice having same ellipticity ratio from the first ring to the last ring. Due to the compactness of design light confinement in PCF is tight than conventional fiber. By examined the simulation result, for wavelength range $1000-1800 \mathrm{~nm}$, designed PCF offer birefringence up to 0.05554 .

## CHAPTER 4

## NUMERICAL ANALYSIS OF SPIRAL PCF

### 4.1 Introduction

In this chapter, two dimensional spiral PCF has been designed using Comsol 5.1. Comsol 5.1 is based on finite element method. [1-5] The Design contains five rings of circular air holes in the spiral. Three configurations of spiral PCF have been analysed for different optical properties such as effective refractive index, dispersion, effective area etc. In these three configurations, the diameter of air hole is changed and all another parameter like pitch etc. is kept constant. Approaching from circular air hole spiral PCF to elliptical air hole spiral PCF, air filling fraction is kept same and the results compared for each design. [20-21]

### 4.2 Design Parameter of Circular spiral PCF

| NAME | VALUE | DISCRIPTION |
| :---: | :--- | :--- |
| d | $1,0.8,0.8[\mu \mathrm{~m}]$ | Diameter of air hole |
| $\mathrm{r}_{0}$ | $2[\mu \mathrm{~m}]$ | Radius of first air hole |
| $\mathrm{r}_{1}$ | $3.8[\mu \mathrm{~m}]$ | Radius of second air <br> hole |
| $\mathrm{r}_{2}$ | $5.6[\mu \mathrm{~m}]$ | Radius of third air hole |
| $\mathrm{r}_{3}$ | $7.4[\mu \mathrm{~m}]$ | Radius of fourth air hole |
| $\mathrm{r}_{4}$ | $9.2[\mu \mathrm{~m}]$ | Radius of fifth air hole |
| W | $1.55[\mu \mathrm{~m}]$ | wavelength |
| f | C_const/w | frequency |
| $\mathrm{n}_{\text {core }}$ | 1.45 | Refractive index |
| $\mathrm{n}_{\text {air hole }}$ | 1 | Refractive index |

### 4.3Geometry of Circular air hole spiral PCF



Figure 4.1 Snap shot of Circular air hole spiral PCF with (a) d=0.6[ $\mu \mathrm{m}]$ (b)d=0.8[ $\mu \mathrm{m}]$

$$
\text { and }(\mathrm{c}) \mathrm{d}=1[\mu \mathrm{~m}]
$$

### 4.4 Snapshot of mode profile



Fig:4.2 (a) $d=1[\mu \mathrm{~m}]$


Fig:4.2 (b) d=0.8[ $\mu \mathrm{m}]$


Fig:4.2 (c) $\mathrm{d}=0.6[\mu \mathrm{~m}]$

Mode profile of Spiral PCF is shown at $1.55 \mu \mathrm{~m}$ wavelength for the fundamental mode. Color variation (red for maximum, blue for minimum power) for power is shown. From this figure, it is shown that maximum light is passed through the core, not in the cladding.

### 4.5 Effective mode index



Figure 4.3 refractive index vs wavelength plot for $\mathrm{d}=1,0.8,0.6[\mu \mathrm{~m}]$
Fig 4.3 shows the variation of effective index with wavelength for different circular air hole spiral PCF. It can be analysed that the slope of Effective refractive index increases with a diameter of air holes. Relation between $n_{\text {eff }}$ and wavelength is given as

$$
\beta=\frac{2 \pi}{\lambda} \times n_{e f f}
$$

From above formula, there is reciprocal relation between $n_{e f f}$ and wavelength and it is verified from the Fig 4.3.

### 4.6 Dispersion profile

Total dispersion is the variation of group velocity with variation in wavelength. Dispersion of PCF is highly effected by the size of air holes and the air hole arrangement in geometry. Another parameter that can alter dispersion profile is a number of spiral arm and size of the core. From Fig 4.4, it can be analysed that dispersion is minimum for diameter $0.6 \mu \mathrm{~m}$ and maximum for diameter $1 \mu \mathrm{~m}$. Total dispersion (chromatic dispersion) made of two forms of component (1) waveguide dispersion (2) material dispersion [28]


Fig 4.4 Plot of waveguide dispersion $(\mathrm{ps} / \mathrm{nm}-\mathrm{km}) \mathrm{v} / \mathrm{s}$ wavelength for $\mathrm{d}=1[\mu \mathrm{~m}], 0.8$ $[\mu \mathrm{m}] .0 .6[\mu \mathrm{~m}]$.

### 4.7 Effective Area

In Figure 4.5, the effect of diameter of air hole on the effective area is analysed. Effective area linearly increases with wavelength. The effective area of conventional PCF is high over a spiral photonic crystal fiber. This less effective area is an advantage over conventional PCF. Due to the less effective area, this fiber can be used in the nonlinear application. It can be observed from Fig 4.5 that as we increase the diameter of the air hole effective area get reduced and at diameter $1 \mu \mathrm{~m}$ we get low effective area than others. [11]
effective area vs wavelength


Fig:4.5 Plot of Effective Area vs wavelength for $\mathrm{d}=1[\mu \mathrm{~m}], 0.8[\mu \mathrm{~m}], 0.6[\mu \mathrm{~m}]$.

### 4.8 Design Parameters of Elliptical Air hole spiral PCF

| NAME | VALUE | DISCRIPTION |
| :---: | :--- | :--- |
| d | $1[\mu \mathrm{~m}]$ | Diameter of air hole |
| $\mathrm{r}_{0}$ | $2[\mu \mathrm{~m}]$ | Radius of first air hole |
| $\mathrm{r}_{1}$ | $3.8[\mu \mathrm{~m}]$ | Radius of second air hole |
| $\mathrm{r}_{2}$ | $5.6[\mu \mathrm{~m}]$ | Radius of third air hole |
| $\mathrm{r}_{3}$ | $7.4[\mu \mathrm{~m}]$ | Radius of fourth air hole |
| $\mathrm{r}_{4}$ | $9.2[\mu \mathrm{~m}]$ | Radius of fifth air hole |
| w | $1.55[\mu \mathrm{~m}]$ | Wavelength |
| f | $\mathrm{C}_{2}$ const/w | Frequency |
| $\mathrm{n}_{\text {core }}$ | 1.45 | Refractive index of core <br> cladding |
| $\mathrm{n}_{\text {air hole }}$ | 1 | Major axis diameter of elliptical air <br> hole |
| a | $.55[\mu \mathrm{~m}]$ | Minor axis diameter of elliptical air <br> hole |
| b | $.45[\mu \mathrm{~m}]$ |  |

### 4.9 Geometry of elliptical air hole spiral PCF



Figure 4.6 snap shot of elliptical air hole spiral PCF a: major axis b: minor axis of ellipse
Fig 4.6(a) $a=.0 .57[\mu \mathrm{~m}], \mathrm{b}=0.43[\mu \mathrm{~m}]$ Fig 4.6(b) with different ellipticity Fig 4.6(c)

$$
\mathrm{a}=0.62[\mu \mathrm{~m}], \mathrm{b}=0.40
$$

### 4.10 Snapshot of mode profile



Figure 4.7 Snap shot of mode profile for different Elliptical air hole spiral PCF
Fig 4.7(a) $\mathrm{a}=0.57[\mu \mathrm{~m}], \mathrm{b}=0.43[\mu \mathrm{~m}]$ Fig 4.7(b) with different ellipticity Fig 4.7(c)

$$
\mathrm{a}=0.62[\mu \mathrm{~m}], \mathrm{b}=0.40
$$

In given figure, red color shows the maximum intensity of light and blue color shows the minimum intensity of light. From mode profile, we can examine that most of the light is confined in core region due to refractive index variation. Confinement in PCF is high than conventional fiber. This is the advantage of PCF over conventional fiber.[24]

### 4.11 Refractive index vs wavelength

The wavelength is varied from $0.2 \mu \mathrm{~m}$ to $2 \mu \mathrm{~m}$ for the simulation. $\mathrm{n}_{\text {eff }}$ is calculated by simulating the design. The variation in effective refractive index $\mathrm{v} / \mathrm{s}$ wavelength is shown in Fig 4.8. It can be examined from the graph that effective refractive index decreases as the wavelength is increased. From the graph, it observed that the slope of effective refractive index increases with ellipticity ratio.


Figure 4.8(a) Plot of Effective refractive index v/s wavelength for ellipticity ratio

$$
1.22,1.32,1.55
$$



Fig 4.8(b) zoom view of refractive index vs wavelength plot


Fig 4.9(a) Plot of Total dispersion v/s wavelength for ellipticity ratio 1,1.22,1.32,1.64


Fig 4.9(b) Plot showing Flat range of dispersion v/s wavelength
It can be analysed that dispersion is highly affected by the size of air hole so if the air filling fraction is increased or size of air hole is increased the dispersion also changes.

From Fig 4.8 and Fig 4.9, it can be analysed that for ellipticity ratio 1.64 we get the highest dispersion and for graded size air hole we get minimum distortion.So if ellipticity ratio from the first ring to the last ring is increased or decreased the magnitude of dispersion is highly affected. A minimum magnitude of dispersion is obtained for ellipticity ratio 1.22 . From figure 4.9 (b) it can be examined that nearly flat dispersion is obtained from $1.5 \mu \mathrm{~m}$ to $1.68 \mu \mathrm{~m}$ wavelength range. An important fact that can be observed from the Fig 4.9 is that when the geometry is changed from circular to elliptical air holes, the magnitude of dispersion gets increased but birefringence increases. [21]

### 4.13 Birefringence

Birefringence is the difference between the two orthogonal directions. Modal birefringence is defined as [12]

Birefringence $=\left[\mathrm{n}_{\text {eff }}(\mathrm{X}\right.$ mode $)-\mathrm{n}_{\mathrm{eff}}(\mathrm{Y}$ mode $\left.)\right]$


Fig 4.10(a) snap shot of X polarization


Fig 4.10(b) snap shot of $Y$ polarization

Fig 4.10 (a) snap shot of $X$
polarization mode polarization mode


Fig 4.11 Plot of ellipticity ratio vs wavelength
The effect of ellipticity ratio on wavelength is shown in Fig 4.11. It can see from the graph that birefringence varies with ellipticity ratio. In the plot, the ellipticity range is varied from 0.8 to 2.4 and for ellipticity ratio 2.2 , we get the highest value of birefringence.

### 4.15 Birefringence v/s Wavelength

The proposed PCF consists of an elliptical-Spiral arrangement of the air hole. In comparison to conventional PCF structure supporting different properties, the compact design of elliptical air hole spiral PCF achieves large birefringence. From Figure 4.12, it can be seen that birefringence increases linearly with frequency [26]. We get high birefringence for ellipticity ratio 1.64 for wavelength range 1.50 to $1.80 \mu \mathrm{~m}$, designed PCF offered high birefringence up to 0.004 .


Fig 4.12 Plot of Birefringence $\mathrm{v} / \mathrm{s}$ wavelength for different ellipticity ratio

### 4.16 Effective area v/s wavelength plot

From the plot shown in Fig 4.13, the effect of ellipticity ratio on the effective area can be examined. It is observed that effective area of elliptical air hole spiral PCF linearly increases with wavelength. The effective area of elliptical air hole spiral PCF is considerably small than conventional fiber. This property of PCF can be used in various nonlinearity application such as supercontinuum generation, four waves mixing etc. It can be observed from the plot that at ellipticity ratio 1.55 , the effective area is lowest as compared others.


Fig 4.13(a) Effective area v/s wavelength plot


Fig 4.13 (b) zoom view of Effective area v/s wavelength p

## CHAPTER 5

## COMPARATIVE STUDY AND CONCLUSION

### 5.1 Introduction

This chapter deals with the comparative analysis of different characterstics of spiral photonic crystal fiber like effective mode index, waveguide dispersion and chromatic dispersion by varying wavelength for different diameter of air hole spiral photonic crystal fiber.[15]

### 5.2 Comparison of Effective mode index

Fig 4.19 shows the comparative study of effective mode index. In Fig 4.19 it can be seen that as the wavelength is increased the value of $n_{\text {eff }}$ decreases. Fig 4.19 shows that the slope of refractive index $\mathrm{v} / \mathrm{s}$ wavelength plot is maximum for elliptical air hole spiral PCF as compared with circular air hole PCF.

Table 5.1 Wavelength v/s effective refractive index

| wavelength | $\mathrm{a} / \mathrm{b}=1.22$ | $\mathrm{a} / \mathrm{b}$ <br> $=1.32$ | $\mathrm{a} / \mathrm{b}=1.55$ | $\mathrm{a} / \mathrm{b}=\mathrm{graded}$ | neff <br> $\mathrm{d}=1[\mathrm{um}]$ | neff <br> $\mathrm{d}=.8[\mathrm{um}]$ | neff <br> $\mathrm{d}=.6[\mathrm{um}]$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.2 | 1.449166853 | 1.449151 | 1.449173039 | 1.449151355 | 1.449721812 | 1.449743592 | 1.449784087 |
| 0.305882353 | 1.448092071 | 1.448057 | 1.448105572 | 1.448056659 | 1.449360212 | 1.449412177 | 1.449506576 |
| 0.411764706 | 1.446612718 | 1.44655 | 1.446635343 | 1.446550049 | 1.448860308 | 1.448956318 | 1.449127117 |
| 0.517647059 | 1.444752092 | 1.444656 | 1.444785287 | 1.444656022 | 1.448229799 | 1.448384668 | 1.448654858 |
| 0.623529412 | 1.442532128 | 1.442398 | 1.442577074 | 1.442397615 | 1.447476559 | 1.447706235 | 1.448099731 |
| 0.729411765 | 1.439734601 | 1.439578 | 1.440031218 | 1.439796464 | 1.446608729 | 1.446930514 | 1.447472466 |
| 0.835294118 | 1.436747866 | 1.43656 | 1.437167239 | 1.436872939 | 1.445634794 | 1.446067536 | 1.446784355 |
| 0.941176471 | 1.433437125 | 1.43322 | 1.433453364 | 1.433646334 | 1.444563643 | 1.445127821 | 1.446046878 |
| 1.047058824 | 1.429820031 | 1.429578 | 1.429821449 | 1.4301351 | 1.443404583 | 1.444122218 | 1.44527127 |
| 1.152941176 | 1.425914275 | 1.425652 | 1.42589325 | 1.426357078 | 1.442167287 | 1.44306169 | 1.444468127 |
| 1.258823529 | 1.421737785 | 1.421462 | 1.421685639 | 1.422329697 | 1.4408617 | 1.441957056 | 1.443647091 |
| 1.364705882 | 1.417308825 | 1.417026 | 1.41721593 | 1.41807006 | 1.439497899 | 1.440818747 | 1.442816623 |
| 1.470588235 | 1.412645929 | 1.412365 | 1.412501872 | 1.413594847 | 1.438085938 | 1.439656573 | 1.441983883 |
| 1.576470588 | 1.40776757 | 1.407497 | 1.407561426 | 1.408919975 | 1.436635675 | 1.438479534 | 1.441154705 |


| 1.682352941 | 1.402691513 | 1.402442 | 1.402412262 | 1.404059973 | 1.435156604 | 1.437295687 | 1.440333644 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.788235294 | 1.397433823 | 1.397214 | 1.397070941 | 1.399027094 | 1.433657705 | 1.436112051 | 1.439524076 |
| 1.894117647 | 1.392007662 | 1.391827 | 1.391551818 | 1.393830249 | 1.432147303 | 1.434934579 | 1.438728337 |



Fig 5.1(a) comparision of $n_{e f f} \mathrm{v} / \mathrm{s}$ wavelength for diameter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$


Fig 5.1(b) Zoom View of Fig 5.1(a)

## 5.3 comparision of waveguide dispersion

Fig 5.20 shows a variation of dispersion with wavelength and it can be seen from the graph that as we increase the diameter of airhole dispersion also increases.


Fig 5.2 waveguide dispersion $\mathrm{v} / \mathrm{s}$ wavelength for dimeter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$

## 5.4 comparision of chromatic dispersion(total dispersion) Table 5.2 Wavelength v/s total dispersion

| wavelength | $\mathrm{a} / \mathrm{b}=1.32$ | $\mathrm{a} / \mathrm{b}=1.22$ | $\mathrm{a} / \mathrm{b}=1.64$ | mix | $\mathrm{a} / \mathrm{b}=1.0 \mathrm{um}$ <br> circular | $\mathrm{d}=0.6 \mathrm{um}$ | $\mathrm{D}=0.8 \mathrm{um}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.517647059 | $631.8940409$ | $631.8957836$ | -641.136751 | -640.304876 | $677.5611786$ | $683.7168533$ | -680.024165 |
| 0.623529412 | $245.4728624$ | $246.3333746$ | -261.64019 | -260.833925 | $303.2061562$ | $311.0864995$ | -306.422742 |
| 0.729411765 | $104.0996341$ | $104.1374419$ | -104.299298 | -103.525587 | $150.5085352$ | -160.312355 | -154.600807 |
| 0.835294118 | $34.54773613$ | $34.51025927$ | 16.39738005 | -30.2269825 | $81.43242087$ | $93.27491991$ | -86.5129079 |
| 0.941176471 | 22.76285561 | 21.73327127 | 85.41220659 | 16.72897307 | $38.38854081$ | $52.24782281$ | -44.5331464 |
| 1.047058824 | 50.93237015 | 49.38628283 | 86.46978143 | 44.17308078 | $14.57959505$ | $30.26835016$ | -21.8043405 |
| 1.152941176 | 75.63847525 | 73.52690224 | 90.89383425 | 68.36791401 | 6.258813238 | $10.90495025$ | -1.98725523 |
| 1.258823529 | 94.46920131 | 91.75597403 | 99.21576505 | 86.96833067 | 21.79047736 | 3.65205423 | 12.66207736 |


| 1.364705882 | 105.0723451 | 101.7400514 | 110.5827549 | 97.69374364 | 29.70546452 | 11.20029635 | 19.90978681 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.470588235 | 116.1491334 | 112.2145752 | 122.3159461 | 109.3133502 | 38.64923401 | 20.44435016 | 28.46475035 |
| 1.576470588 | 116.3013997 | 111.8417734 | 122.8905755 | 110.4779158 | 36.99938551 | 19.76981603 | 26.74891725 |
| 1.682352941 | 116.2271908 | 111.4052306 | 122.8489322 | 111.9023659 | 35.01027064 | 19.3916755 | 25.03795682 |
| 1.788235294 | 116.6914955 | 111.7601394 | 122.8176309 | 114.3325155 | 32.80046206 | 19.35024654 | 23.44774087 |
| 1.894117647 | 133.2507909 | 128.3315139 | 138.7569288 | 132.6238378 | 45.5178704 | 33.83913783 | 36.69932799 |



Fig 5.3 comparision of chromatic dispersion v/s wavelength
Chromatic dispersion is a combination of two type of dispersion 1) waveguide dispersion 2) material disersion. Dispersion in PCF is highly effected by the size of air holes and arrangement of air hole in cladding region. The dispersion propery can be altered by changing the geometry of PCF. Fig 5.3 shows the variation of dispersion with wavelength, it can be observed from the Fig 5.3 that the magnitude of dispersion is minimum for circular air hole spiral PCF and higher for eliptical air hole spiral PCF. At $1.55 \mu \mathrm{~m}$, the minimum dispersion obtained for $0.6 \mu \mathrm{~m}$ circular air hole.By comparing the result of circular air hole spiral PCF for diameter $1 \mu \mathrm{~m}$ and elliptical air hole spiral PCF for same air filling fraction, we get lower dispersion for circular air hole spiral PCF.

### 5.5 Comparison of zero dispersion wavelength <br> Table 5.3 Zero dispersion wavelength

| Circular air hole | Zero dispersion <br> wavelength | Elliptical air hole | Zero dispersion <br> wavelength |
| :--- | :--- | :--- | :--- |
| Diameter <br> $[\mu \mathrm{m}]$$=1.0$ | $1.12[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.22$ | $0.901[\mu \mathrm{~m}]$ |
| Diameter <br> $[\mu \mathrm{m}]$$=0.8$ | $1.18[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.32$ | $0.896[\mu \mathrm{~m}]$ |
| Diameter <br> $[\mu \mathrm{m}]$$=0.6$ | $1.24[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.62$ | $0.835[\mu \mathrm{~m}]$ |
|  | Ellipticity <br> ratio=graded | $0.903[\mu \mathrm{~m}]$ |  |



Fig 5.4(a) zero dispersion wavelength at diameter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$


Fig 5.4(b) zoom view of above graph
the zero-dispersion wavelength is the wavelength at which waveguide dispersion and material dispersion and cancel one another. it can be seen from fig 5.4(b) that as reduce the diameter of air hole zero dispersion wavelength shift toward right hand side. By analyzing the result of both designs, it observes that as change the geometry of air holes from circular to elliptical, zero dispersion wavelength get shifted to the lower side of wavelength. [23]

### 5.6 Comparison of effective area

Table 5.4 Wavelength v/s effective area

| w[ $\mu \mathrm{m}$ ] | $a / b=1.22$ | $a / b=1.32$ | $\mathrm{a} / \mathrm{b}=1.55$ | graded | $\mathrm{d}=1 \mathrm{um} \mathrm{c}$ | $\begin{aligned} & \mathrm{d}=0.8 \mathrm{um} \\ & \mathrm{c} \end{aligned}$ | d=0.6 c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.2 | $\begin{aligned} & \hline 3.77213 \\ & 1186 \end{aligned}$ | $\begin{array}{\|l\|} \hline 3.78641 \\ 5948 \\ \hline \end{array}$ | $\begin{aligned} & 3.76221 \\ & 508 \end{aligned}$ | $\begin{aligned} & 3.89639 \\ & 6857 \end{aligned}$ | $\begin{aligned} & 3.82307 \\ & 1697 \end{aligned}$ | $\begin{aligned} & \hline 4.42673 \\ & 5403 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.14322 \\ & 8341 \end{aligned}$ |
| $\begin{aligned} & 0.30588 \\ & 2353 \end{aligned}$ | $\begin{aligned} & 3.84969 \\ & 0648 \end{aligned}$ | $\begin{aligned} & \hline 3.86429 \\ & 3064 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.83991 \\ & 9906 \end{aligned}$ | $\begin{aligned} & 3.97183 \\ & 1001 \end{aligned}$ | $\begin{aligned} & 3.89276 \\ & 7746 \end{aligned}$ | $\begin{aligned} & 4.50645 \\ & 0938 \end{aligned}$ | $\begin{aligned} & 5.25345 \\ & 5655 \end{aligned}$ |
| $\begin{aligned} & \hline 0.41176 \\ & 4706 \end{aligned}$ | $\begin{aligned} & \hline 3.92790 \\ & 0397 \end{aligned}$ | $\begin{aligned} & 3.94271 \\ & 0503 \end{aligned}$ | $\begin{aligned} & 3.91775 \\ & 6542 \end{aligned}$ | $\begin{aligned} & 4.04791 \\ & 7293 \end{aligned}$ | $\begin{aligned} & \hline 3.96340 \\ & 9882 \end{aligned}$ | $\begin{aligned} & \hline 4.58807 \\ & 1714 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.37541 \\ & 498 \end{aligned}$ |
| $\begin{aligned} & 0.51764 \\ & 7059 \end{aligned}$ | $\begin{aligned} & 4.00734 \\ & 6111 \end{aligned}$ | $\begin{array}{\|l\|} \hline 4.02214 \\ 8574 \end{array}$ | $\begin{aligned} & 3.99638 \\ & 1016 \end{aligned}$ | $\begin{aligned} & 4.12457 \\ & 6639 \end{aligned}$ | $\begin{aligned} & 4.03518 \\ & 0071 \end{aligned}$ | $\begin{aligned} & \hline 4.67239 \\ & 4294 \end{aligned}$ | $\begin{aligned} & 5.51534 \\ & 3806 \end{aligned}$ |


| 0.62352 | 4.08922 | 4.10389 | 4.07663 | 4.20235 | 4.10855 | 4.76043 | 5.68245 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 9412 | 9882 | 3848 | 0939 | 9198 | 3734 | 7539 | 269 |
| 0.72941 | 4.11849 | 4.19000 | 4.15983 | 4.28206 | 4.18377 | 4.85359 | 5.89002 |
| 1765 | 8296 | 1386 | 2827 | 7549 | 514 | 7558 | 2937 |
| 0.83529 | 4.19897 | 4.20942 | 4.24906 | 4.36532 | 4.26114 | 4.95402 | 6.15614 |
| 4118 | 0615 | 438 | 3148 | 8268 | 6999 | 3671 | 4673 |
| 0.94117 | 4.28626 | 4.29653 | 4.25032 | 4.45615 | 4.34110 | 5.06505 | 6.50405 |
| 6471 | 6404 | 8583 | 8471 | 9114 | 3581 | 3793 | 4728 |
| 1.04705 | 4.38350 | 4.39408 | 4.34403 | 4.56428 | 4.42428 | 5.19168 | 6.96196 |
| 8824 | 3932 | 7191 | 6914 | 1211 | 7177 | 4424 | 707 |
| 1.15294 | 4.49535 | 4.50690 | 4.45157 | 4.71069 | 4.51168 | 5.34103 | 7.56225 |
| 1176 | 4449 | 4522 | 8296 | 5973 | 719 | 4793 | 5223 |
| 1.25882 | 4.62853 | 4.64188 | 4.57920 | 4.93502 | 4.60482 | 5.52275 | 8.33983 |
| 3529 | 2812 | 9572 | 1431 | 3101 | 817 | 0946 | 6175 |
| 1.36470 | 4.79246 | 4.80871 | 4.73559 | 5.30575 | 4.70600 | 5.74929 | 9.32966 |
| 5882 | 0576 | 8265 | 6964 | 9001 | 2609 | 0284 | 4759 |
| 1.47058 | 5.00025 | 5.02088 | 4.93277 | 5.94694 | 4.81854 | 6.03603 | 10.5634 |
| 8235 | 413 | 2095 | 2544 | 723 | 1391 | 0659 | 1686 |
| 1.57647 | 5.27017 | 5.29714 | 5.18724 | 7.13682 | 4.94710 | 6.40116 | 12.0657 |
| 0588 | 3552 | 2956 | 9215 | 0457 | 728 | 3022 | 5651 |
| 1.68235 | 5.62758 | 5.66344 | 5.52163 | 8.75949 | 5.09798 | 6.86534 | 13.8508 |
| 2941 | 8888 | 3122 | 4868 | 7803 | 7091 | 5171 | 8964 |
| 1.78823 | 6.10742 | 6.15522 | 5.96656 | 10.5745 | 5.27934 | 7.45107 | 14.9262 |
| 5294 | 3164 | 2861 | 4693 | 7026 | 7959 | 4732 | 2588 |
| 1.89411 | 6.75682 | 6.81984 | 6.56280 | 12.5865 | 5.50141 | 8.18175 | 14.9987 |
| 7647 | 8862 | 9249 | 3146 | 1604 | 6427 | 6249 | 1432 |
|  |  |  |  |  |  |  |  |



Figure 5.5 comparison of Effective area vs wavelength plot
In Fig 5.5, the effect of diameter of air hole and geometry of air hole on the effective area is examined. The effective area of PCF is much smaller than conventional PCF. By analyzing the result of PCF, it is observed that elliptical air hole PCF offers high effective area than circular air hole PCF. For circular air hole PCF of diameter $1 \mu \mathrm{~m}$, a minimum effective area is obtained.

### 5.7 Birefringence vs Wavelength

. High birefringence fiber can be used as a sensor. To increase the birefringence, elliptical air holes are introduced in PCF or the symmetry of PCF is broken. It can be seen from Fig 5.6 that birefringence varies with ellipticity ratio. Because if, there is a change in ellipticity ratio air filling fraction get changed. It can be seen from the graph that for circular air hole minimum birefringence of the order $10^{-3}$ is observed and as the ellipticity ratio is increased, the magnitude of birefringence for PCF also increases.

Table 5.5 Wavelength v/s birefringence

| Waveleng th | $a / b=1.22$ | $a / b=1.32$ | $a / b=1.55$ | $a / b=1.64$ | graded ellip holes | circular air hole |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.2 | $\begin{aligned} & 1.74847 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 1.50167 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 2.80366 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 3.14214 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 4.19246 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 4.19467 \mathrm{E}- \\ & 06 \end{aligned}$ |
| $\begin{aligned} & 0.3058823 \\ & 53 \end{aligned}$ | $\begin{aligned} & 1.48852 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.46567 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.77249 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.85311 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.78522 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.78587 \mathrm{E}- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.4117647 \\ & 06 \end{aligned}$ | $\begin{aligned} & 4.26633 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.29268 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.84759 E- \\ & 05 \end{aligned}$ | $\begin{aligned} & 5.0027 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.39874 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.39995 E- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.5176470 \\ & 59 \end{aligned}$ | $\begin{aligned} & 8.78263 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 8.92817 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 9.85487 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 0.0001013 \\ & 6 \end{aligned}$ | $\begin{aligned} & 8.50137 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 8.50318 \mathrm{E}- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.6235294 \\ & 12 \end{aligned}$ | $\begin{aligned} & 0.0001526 \\ & 41 \end{aligned}$ | $\begin{aligned} & 0.0001562 \\ & 27 \end{aligned}$ | $\begin{aligned} & 0.0001711 \\ & 26 \end{aligned}$ | $\begin{aligned} & 0.0001759 \\ & 51 \end{aligned}$ | $\begin{aligned} & 0.0001427 \\ & 72 \end{aligned}$ | $\begin{aligned} & 0.0001427 \\ & 97 \end{aligned}$ |
| $\begin{aligned} & 0.7294117 \\ & 65 \end{aligned}$ | $\begin{aligned} & 0.0002389 \\ & 6 \end{aligned}$ | $\begin{aligned} & 0.0002458 \\ & 88 \end{aligned}$ | $\begin{aligned} & 0.0002690 \\ & 52 \end{aligned}$ | $\begin{aligned} & 0.0002768 \\ & 75 \end{aligned}$ | $\begin{aligned} & 0.0002184 \\ & 91 \end{aligned}$ | $\begin{aligned} & 0.0002185 \\ & 21 \end{aligned}$ |
| $\begin{aligned} & 0.8352941 \\ & 18 \end{aligned}$ | $\begin{aligned} & 0.0003481 \\ & 86 \end{aligned}$ | $\begin{aligned} & 0.0003599 \\ & 85 \end{aligned}$ | $\begin{aligned} & 0.0003948 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0004068 \\ & 56 \end{aligned}$ | $\begin{aligned} & 0.0003127 \\ & 74 \end{aligned}$ | $\begin{aligned} & 0.0003128 \\ & 07 \end{aligned}$ |
| $\begin{aligned} & 0.9411764 \\ & 71 \end{aligned}$ | $\begin{aligned} & 0.0004812 \\ & 57 \end{aligned}$ | $\begin{aligned} & 0.0004998 \\ & 25 \end{aligned}$ | $\begin{aligned} & 0.0005505 \\ & 49 \end{aligned}$ | $\begin{aligned} & 0.0005683 \\ & 25 \end{aligned}$ | $\begin{aligned} & 0.0004256 \\ & 15 \end{aligned}$ | $\begin{aligned} & 0.0004256 \\ & 48 \end{aligned}$ |
| $\begin{aligned} & 1.0470588 \\ & 24 \end{aligned}$ | $\begin{aligned} & 0.0006386 \\ & 42 \end{aligned}$ | $\begin{aligned} & 0.0006662 \\ & 97 \end{aligned}$ | $\begin{aligned} & 0.0007380 \\ & 86 \end{aligned}$ | $\begin{aligned} & 0.0007634 \\ & 49 \end{aligned}$ | $\begin{aligned} & 0.0005564 \\ & 16 \end{aligned}$ | $\begin{aligned} & 0.0005564 \\ & 48 \end{aligned}$ |
| $\begin{aligned} & 1.1529411 \\ & 76 \end{aligned}$ | $\begin{aligned} & 0.0008203 \\ & 19 \end{aligned}$ | $\begin{aligned} & 0.0008598 \\ & 38 \end{aligned}$ | $\begin{aligned} & 0.0009588 \\ & 7 \end{aligned}$ | $\begin{aligned} & 0.0009940 \\ & 67 \end{aligned}$ | $\begin{aligned} & 0.0007040 \\ & 13 \end{aligned}$ | $\begin{aligned} & 0.0007040 \\ & 39 \end{aligned}$ |
| $\begin{aligned} & 1.2588235 \\ & 29 \end{aligned}$ | $\begin{aligned} & 0.0010256 \\ & 88 \end{aligned}$ | $\begin{aligned} & 0.0010803 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0012138 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0012615 \\ & 02 \end{aligned}$ | $\begin{aligned} & 0.0008667 \\ & 06 \end{aligned}$ | $\begin{aligned} & 0.0008666 \\ & 51 \end{aligned}$ |
| $\begin{aligned} & 1.3647058 \\ & 82 \end{aligned}$ | $\begin{aligned} & 0.0012533 \\ & 52 \end{aligned}$ | $\begin{aligned} & 0.0013267 \\ & 15 \end{aligned}$ | $\begin{aligned} & 0.0015029 \\ & 07 \end{aligned}$ | $\begin{aligned} & 0.0015661 \\ & 58 \end{aligned}$ | $\begin{aligned} & 0.0010422 \\ & 92 \end{aligned}$ | $\begin{aligned} & 0.0010418 \\ & 17 \end{aligned}$ |
| $\begin{aligned} & 1.4705882 \\ & 35 \end{aligned}$ | $\begin{aligned} & 0.0015006 \\ & 71 \end{aligned}$ | $\begin{aligned} & 0.0015965 \\ & 73 \end{aligned}$ | $\begin{aligned} & 0.0018244 \\ & 43 \end{aligned}$ | $\begin{aligned} & 0.0019066 \\ & 77 \end{aligned}$ | $\begin{aligned} & 0.0012281 \\ & 34 \end{aligned}$ | $\begin{aligned} & 0.0012261 \\ & 81 \end{aligned}$ |
| 1.5764705 | 0.0017629 | 0.0018847 | 0.0021733 | 0.0022782 | 0.0014213 | 0.0014151 |


| 88 | 22 | 75 | 81 | 2 | 25 | 78 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1.6823529 \\ & 41 \end{aligned}$ | $\begin{aligned} & 0.0020319 \\ & 75 \end{aligned}$ | $\begin{aligned} & 0.0021818 \\ & 62 \end{aligned}$ | $\begin{aligned} & 0.0025389 \\ & 63 \end{aligned}$ | $\begin{aligned} & 0.0026698 \\ & 45 \end{aligned}$ | $\begin{aligned} & 0.0016190 \\ & 21 \end{aligned}$ | $\begin{aligned} & 0.0016024 \\ & 97 \end{aligned}$ |
| $\begin{aligned} & 1.7882352 \\ & 94 \end{aligned}$ | $\begin{aligned} & 0.0022953 \\ & 31 \end{aligned}$ | $\begin{aligned} & 0.0024735 \\ & 5 \end{aligned}$ | $\begin{aligned} & 0.0029046 \\ & 53 \end{aligned}$ | $\begin{aligned} & 0.0030644 \\ & 66 \end{aligned}$ | $\begin{aligned} & 0.0018189 \\ & 35 \end{aligned}$ | $\begin{aligned} & 0.0017793 \\ & 89 \end{aligned}$ |
| $\begin{aligned} & 1.8941176 \\ & 47 \end{aligned}$ | $\begin{aligned} & 0.0025385 \\ & 98 \end{aligned}$ | $\begin{aligned} & 0.0027456 \\ & 21 \end{aligned}$ | $\begin{aligned} & 0.0032560 \\ & 59 \end{aligned}$ | $\begin{aligned} & 0.0034475 \\ & 62 \end{aligned}$ | $\begin{aligned} & 0.0020198 \\ & 56 \end{aligned}$ | $\begin{aligned} & 0.0019346 \\ & 94 \end{aligned}$ |



Fig 5.6 birefringence $\mathrm{v} / \mathrm{s}$ frequency plot for different ellipticity ratio

## Conclusion and discussion

Proposed two-dimensional photonic crystal fiber has been designed and analysed for high birefringence and flattened dispersion. For analyzing the proposed design Finite Element Method has been used. The following fundamental characteristics of PCFs have been found out. They are shown in tabular format.

## Our finding

| 1.Power confinement of spiral PCF for different diameter in circular spiral PCF |
| :--- |
| 2.Effective mode index variation with wavelength for different diameter in circular <br> spiral PCF |
| 3.Material dispersion for diffused silica at refractive index 1.45 in circular spiral PCF |
| 4. Wavefuide dispersion for circular hole PCF at different diameter by varying <br> wavelength |
| 5.Chromatic dispersion for circular hole PCF at different diameter by varying <br> wavelength |
| 6.Zero dispersion wavelength at different diameter for circular spiral PCF |
| 7.New structure of elliptical hole spiral PCF keeping all parameter similar |
| 8.Effective refractive index variation v/s wavelength for elliptical hole spiral PCF |
| 9.Chromatic dispersion vs wavelength for elliptical hole spiral PCF |
| 10.Birefringence vs ellipticity ratio for elliptical hole spiral PCF |
| 11.Birefringence vs wavelength plot for elliptical hole spiral PCF |
| 12.Effective area vs wavelength plot for elliptical hole spiral PCF |
| 13.Comparative study of different diameter circular air hole spiral photonic crystal fiber <br> and different ellipticity ratio spiral PCF |

Here It, found out properties of different diameter of air hole for doped silica spiral photonic crystal fiber. In this report, different spiral photonic crystal fiber has been examined. By optimizing the geometry of PCF, we get almost flat dispersion in the range of $1.45[\mathrm{um}]$ to 1.70 [um]. The numerically simulated result shows that a significantly lower dispersion occurs at a diameter of $0.6 \mu \mathrm{~m}$. a circular spiral PCF has been designed in which we increase the diameter of air hole and analyzed that as reduce
the diameter of air hole dispersion also decreases and It also get the zero-dispersion wavelength shift toward right hand side as we reduce the diameter of the air hole. the designed structure also has lower dispersion than octagonal photonic crystal fiber. Due to lower dispersion, the fiber has its prominence in dispersion flatter device application. For further improvement of the result of PCF, move from spiral circular hole to elliptical air hole spiral PCF. Due to the compactness of design, PCF offers high nonlinearity, birefringence, and low effective area. From simulation result, it observes that if increase ellipticity ratio from 1 to 1.64 , dispersion will also increase.it can be examined from the result that birefringence of order 0.003 at $1.80 \mu \mathrm{~m}$ and 0.002 at $1.55 \mu \mathrm{~m}$ is observed and Birefringence also increase with ellipticity ratio and at ellipticity ratio 1.64 , birefringence of order 0.003 is observed. It observed that effective area increases with wavelength and get lower effective area for ellipticity ratio 1.55.but if compare circular air hole PCF and elliptical air hole PCF, circular air hole PCF offer lower effective area.

## Future work

Present Research work on photonic crystal fibers is based on different spiral PCF. By changing the geometry of spiral PCF and air holes ellipticity ratio, the range of flattened dispersion will be increased to significant label and birefringence will be improved. Dispersion engineering is possible in PCFs in the range unachievable for classical fibers (flat dispersion in the large range, zero-dispersion, and anomalous dispersion in the visible range).

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## List of Publications

## Conference Paper

[1] Julie Devi, Amritveer Kaur, Ritu Sharma, Varshali Sharma, Santosh Chaudhary (2017) "Design and Analysis of Spiral Photonic Crystal Fiber giving Ultra Flattened Dispersion for C+L+U Band" International Conference on Optical \& Wireless Technologies (OWT2017) March 18-19, Jaipur
[2] Amritveer Kaur, Julie Devi, Ritu Sharma, Varshali Sharma, Santosh Chaudhary (2017) "Design of Octagonal and Decagonal lattice Photonic Crystal Fiber for achieving Ultra Low flattened dispersion" International Conference on Optical \& Wireless Technologies (OWT2017) March 18-19, Jaipur

# Thesis <br> by Julie Devi 

$\square$

## CHAPTER - 1

## INTRODUCTION

### 1.1 Introduction

Since the introduction of conventional step index fibers, optical fibers have evolved into many forms in the 70s and later single material fiber where effective cladding structures determined the propagation of light. The principle objective was the transportation of light from one point to another whether by step index confinement or by band-gap confinement such as in Bragg fiber. We can use optical fiber in many applications like transporting high speed data, bio sensors Etc. the optical fiber can also use in Gas sensing application, strain or pressure measurement in bridges and highpower amplifier. Photonic Crystal Fibers (PCF) is a variant of the micro structured fibers with greater control of guiding properties. Such a vital Photonic Crystal fiber have large application area in nonlinear devices and high power optical fiber amplifier.

### 1.2History of PCF

Optical fibers were discovered in the 1970s and are now the backbone of opticalcommunication systems due to a large amount of information they can handle. Particularly designed optical fibers are also used ${ }_{21}$ many optical applications, including sensors, medicine, illumination and much more. Standard step-index optical fibers guide light through total internal reflection, which occurs only if the core has a larger refractive index than the outer cladding. The optical signal propagates in the core is completely reflected at the interface core/cladding and is, therefore guided in the core. First fiber is fabricated by Russell consist hexagonal lattice in silica fiber. These novel periodic structures were called photonic crystals. Only light with certain wave vectors can propagate in the structure If a defect or periodic structure is introduced in the is in the structure, the wavelengths forbidden in the periodic structure are now allowed to "stay" in the defect as the photonic crystal running along the air hole prevents them from "escaping". The refractive index is not required to be higher than that of the periodic
material. By using this idea light can be trapped inside a hollow core (defect). Therefore, light can even be guided in the air.[8]

## Theory of PCF

In the last decade, photonic crystal fibers have been under rigorous study and due to the development of PCF and unique application, attracted huge research interest. PCF is a fiber which contains its different optical properties from particularly varying the design and arrangement of air holes in fiber which run through the length of the fiber, not from different glass composition. The simplest type of PCF has triangular lattice. Photonic crystal fiber is categorized into two types of mechanism 1) Photonic band Gap 2) Total Internal reflection


Fig 2.1 geometry of hexagonal PCF

### 1.3.1 Advantage of Photonic Crystal Fiber

> Better light confinement than conventional fibers
> Low dispersion
> Very low attenuation (holey fiber)
> More flexible than conventional fibers
> Many core fiber

### 1.3.2 Basics equations

Propagation of light in PCFs is described by Maxwell's equations. For no free charge or current, the following equations become applicable

$$
\begin{gather*}
\nabla \cdot D=0 \\
\nabla \times H=\frac{\partial D}{\partial t} \\
\nabla \cdot B=0 \\
\nabla \times E=-\frac{\partial B}{\partial t}  \tag{2.1}\\
\varepsilon(\mathrm{r}, \omega)=\varepsilon(\mathrm{r}) \in R \\
\mathrm{D}(\mathrm{r})=\varepsilon(r) \times \varepsilon o \times E(r) \\
\mathrm{B}=\mu O \times H \tag{2.2}
\end{gather*}
$$

Inserting equation b into a

$$
\begin{gather*}
\nabla . \varepsilon(r) \times \epsilon o \times E(r, t)=0 \\
\nabla \times H(r, t)=\varepsilon(r) \times \varepsilon o \times \frac{\partial E(r, t)}{\partial t} \\
\nabla \cdot \mu o . H(r, t)=0  \tag{2.3}\\
\nabla \times E(r, t)=-\mu o \cdot \frac{\partial H(r, t)}{\partial t}
\end{gather*}
$$

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Since Maxwell's equations are linear we can separate out the time dependence by expanding into
a set of harmonic modes

$$
\begin{aligned}
& H(r, t)=H(r) \cdot e^{j \omega t} \\
& E(r, t)=E(r) \cdot e^{j \omega t}
\end{aligned}
$$

To obtain coupled equations we need the following ones

$$
\begin{gather*}
\nabla \cdot \varepsilon(r) \cdot E(r)=0  \tag{2.4}\\
\nabla \times H(r, t)=j \omega \varepsilon(r) \varepsilon o E(r) \\
\nabla \cdot H(r)=0 \\
\nabla \times E(r)=j \omega \cdot \mu o \cdot H(r) \tag{2.5}
\end{gather*}
$$

### 1.4 Guiding mechanism in PCF <br> 1.4.1 Total internal reflection

5
In solid core PCE light, is comes from high refractive index core to lower refractive index cladding ${ }_{33}$ ight is kept in the core by total internal reflection in photonic crystal fiber. In PCF, When the angle of incident is greater is greater than the critical angle, total internal reflection takes place in solid core fiber.
1.4.2 Photonic bandgap in photonic crystal fiber defects is created by introducing air hole in fiber and the photonic band gap is created.in this case light guidance mechanism is like electron conduction mechanism in solid-state physics. Photonic band 63 gap structure offer opportunity to design new optical property in existing fiber. Due to the presence of air hole, light is confined in the core region and these modes guided along the defect through the fiber.

## $1.5 P_{32}$ erties of PCF

### 1.5.1 Confinement loss

The losses in PCFs occur for many reasons, such ${ }_{5}$ Rayleigh scattering loss, intrinsic material absorption loss, macro and micro binding loss, and so on. Fabrication related losses can be reduced by carefully optimizing the fabrication process. The Periodic arrangement of air holes in PCF causes a decrease in optical confinement, is called Confinement loss. PCF is made by single material and so guided mode is leaky. The region of loss is that the 40 active index of the core is iome the refractive index of the cladding. Confinement loss depends on the structure and arrangement of air holes in PCF. We can alter the value of loss by changes the geometry of fiber. For analyzing the
confinement loss, PML layer is applied to PCF. With the help of PML layer, we find the value of the imaginary refractive index and find the confinement loss.

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$$
\begin{equation*}
\text { Confinement loss }=8.686 \times 10^{6} \times \text { ko } \times \mathrm{im}\left(\mathrm{n}_{\mathrm{eff}}\right) \tag{dB/m}
\end{equation*}
$$

### 1.5.2 Normalized frequency

The V parameter (normalized frequency) is commonly used in the design of conventional SIFs and is given by

$$
V=\frac{2 \pi \mathrm{a}}{\lambda} \times \sqrt{\mathrm{n}_{\mathrm{co}}^{2}}-\mathrm{n}_{\mathrm{cl}}^{2}
$$

To finding the V parameter for PCF , its different nature is considered. V parameter of PCF given as

$$
V_{\mathrm{PCF}}=\frac{2 \pi \mathrm{a}}{\mathrm{w}} \times \sqrt{\mathrm{n}_{\mathrm{FM}}^{2}}(\mathrm{w})-\mathrm{n}_{\mathrm{FSM}}^{2}(\mathrm{w})
$$

Where $n_{F M}(w)$ is wavelength dependent refractive index of fundamental mode and $n_{F S M}^{2}(\mathrm{w})$ is fundamental space filling factor. For single mode fiber $V_{\mathrm{PCF}}$ should be equal to $\pi$.

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### 1.5.3 Effective modal area

The effective mode area $A_{\text {eff }}$, is computed using transverse electric or magnetic field vector of the whole cross-sectional area of the fiber. The effective area of the of the fiber core $A_{\text {eff }}$ is defined as [2]

$$
A_{e f f}=\frac{\left(\circlearrowleft \mid E_{t \mid}^{2} d x d y\right)^{2}}{\int \mid E_{t \mid}^{4} d x d y}
$$

Or

$$
A_{e f f}=\frac{\left(\prod \mid H_{t \mid}^{2} d x d y\right)^{2}}{\int \cap H_{t \mid}^{4} d x d y}
$$

where $E_{t}$ and $H_{t}{ }^{7}$ is the transverse electric field vector and magnetic field vector respectively and the integration is done through the whole cross-sectional area of the fiber.

### 1.5.4 Chromatic dispersion

Effective refractive index of mode profile depends on wavelength. Relation between wavelength and refractive index is given by equation below

$$
\mathrm{v}=\frac{c}{n}
$$

All optical source used for optical transmission emit light, in the band of spectral width $\Delta \lambda$, distributed around $\lambda$.so individual frequency component experienced different velocity so different frequency component travel with different speed and pulse get dispersed. The speed at which light travel through fiber rely on its wavelength and design of fiber thus some wavelength of band of which the pulse is embraced may be delayed compared with other, leading to pulse spreading with time after traversing a significant length of fiber called chromatic(Total) dispersion. Total dispersion is the $7{ }_{7} \mathrm{~m}$ of two form of dispersion (1) material dispersion (2) waveguide dispersion. The chromatic dispersion $D$ of a PCF is calculated from given formula [18-20]

$$
\mathrm{D}=-\frac{\lambda}{\mathrm{c}} \times \frac{\mathrm{d}_{\mathrm{neff}}^{2}}{\mathrm{~d} \lambda^{2}}
$$

35 where c is the velocity of light in a vacuum $\mathrm{n}_{\text {eff }}$ is effective refractive index of PCF.

## 52 <br> 1.5.4.1 Material dispersion

The material refractive index depends on the value of wavelength. Material dispersion is calculated by a sellmeier equation which gives the relation between refractive index and wavelength. Usual form of equation is given as [22]

$$
n^{2}(w)=1+\frac{B_{1} w^{2}}{w^{2}-C_{1}}+\frac{B_{2} w^{2}}{w^{2}-C_{2}}+\frac{B_{3} w^{2}}{w^{2}-C_{3}}
$$

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where n is refractive index of material and w is operating wavelength. Coefficient $\mathrm{B}_{1,2,3}$ and $C_{1,2,3}$ is experimentally examine. The coefficient of the sellmeier equation is different for different material.

### 1.5.4.2 Waveguide dispersion

Waveguide dispersion depends on the fiber refractive index profile. Waveguide dispersion is significant for the fiber having small effective area. Altering the refractive index profile will alter the waveguide dispersion.

$$
\mathrm{D}=\frac{\lambda}{\mathrm{c}} \frac{\mathrm{~d}^{2} \mathrm{n}}{\mathrm{~d} \lambda^{2}}
$$

### 1.5.5 Modal birefringence

Effective index profile sometimes depends on the polarization and propagation direction of optical signal. Se the refractive index of the two fundamental modes ( x and y mode) will not be same. Birefringence is the difference of effective refractive index between these two-fundamental modes. Birefringence can be calculated using the equation [9]

$$
\text { Birefringence }=\left[\mathrm{n}_{\text {eff }}(\mathrm{X} \text { mode })-\mathrm{n}_{\text {eff }}(\mathrm{Y} \text { mode })\right]
$$

### 1.5.6 Non-linearity

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The nonlinear effect in optical fiber occurs due to intensity dependence of refractive index in medium or different scattering phenomenon. Nonlinearity is a most important phenomenon in optical fiber communication and used in various applications such as four-wave mixing, Supercontinuum generation and self-phase modulation. Nonlinearity depends on the type of material and design of fiber. Nonlinearity is calculated with the help of nonlinear coefficient that is different to different materials. [12]

$$
\gamma=\frac{2 \pi}{\lambda} \times \frac{26}{\mathrm{n}_{2}}
$$

where $\mathrm{n}_{2}$ is nonlinear coefficient

### 1.6 Applications of PCF

### 1.6.1 Dispersion compensation Fiber

DCF is a simple and developed technology used in optical communication system. Commercially available DCF can compensate the dispersion of all transmission fiber even for high bit rate and long distance. The newest development in DCF reduced losses and length of optical fiber. This fiber can also be used as dispersion shifted fiber. [33]

### 1.6.2 Polarization maintaining PCF

Optical fiber always shows some amount of birefringence even if PCF has a circular design because in fabrication process there is always some stress or pressure which breaks the symmetry of fiber because of this polarization of light propagating in the fiber regularly changes in an uncontrolled manner. To remove this problem PMF is used. PMF has a high value of birefringence, the polarization of light launched into the fiber is aligned with one of the birefringence axes and polarization is maintained even if the fiber is bent. Due to strong birefringence, the propagation constant of two polarization modes is different so the relative phase of such copropagating modes rapidly drift away so any disturbance in giber does not affect large enough on polarization direction. [32]

### 1.6.3 Hollow core fiber

Hollow core fibers light is guided by using a photonic bandgap structure in place of a traditional total internal reflection. Since most of the optical power propagates through the core region, not cladding region, these fibers are particularly unaffected by nonlinear optical effects. Hollow core fibers can offer other advantages like extremely low loss bends, extreme dispersion values and the ability to modify the core material properties by exchange air for some other gas and HC-PCF can be used as microcell.

### 1.6.4 Fiber laser amplifier

Fiber amplifiers are one of the key components of modern telecommunication. Also, fiber lasers are starting to be more and more important in medicine, spectroscopy, and industry. Compared to conventional solid-state lasers, the great advantage of fiber lasers is their outstanding heat dissipation capability. The fiber laser is insusceptible to thermal lensing and all other temperature properties. The one most important advantage of fiber laser amplifier than a conventional laser is the quality of stream of light which is close to the diffraction limit.

## CHAPTER 2

## ANALYSIS METHOD

### 2.1 Methodology

In general, three methods are utilized to analyze the structure and the properties of photonic crystal fibers. They are

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Effective refractive Index Approach

## Basis-Function Expansion Approach

Numerical Approach

### 2.1.1 Effective Index approach

The first approach developed for PCFs was the effective index approach based on a very simple scalar model using an effective cladding index. In this approach propagation of light is through slab like PCF is commonly describe in terms of refractive indices, we can replace 3D structure by an effective 2D refractive index profile .first, an effective index for the periodically repeated hole-in-silica structure is evaluated and then the microstructured cladding region is replaced by a uniform medium with a properly chosen effective index, resulting in an equivalent step index fiber (SIF) consisting of a core and a cladding region. Using this simple model and the well-established fiber theory, we can obtain a qualitative information about PCFs with perfect hexagonal symmetry. The core is pure silica, but the effective cladding index is determined by using the propagation constant of the lowest-order fundamental mode propagating in the periodically repeated hole-in-silica structure without any defects. The propagating modes in such an infinite cladding material are called space filling modes, the propagation constants of which are strongly dependent on the operating wavelength $\lambda$. The propagation constants of the space-filling modes are usually calculated by solving an approximate scalar-wave equation within a unit cell centered on one of the air holes. By reflection symmetry, the Neumann condition is enforced on each cell edge, namely, the normal derivative of the cladding mode field to the edge must be zero.

### 2.1.2 Basic Function Expansion approach

Although the effective index approach can provide good qualitative information about PCFs, this approach is unable to accurately predict modal properties such as dispersion or birefringence. These quantities depend critically on PCF geometries. An early fullvector model for PCFs has been based on a modal decomposition technique using various basis functions such as sinusoidal functions, Hermite-Gaussian functions and cylindrical functions. The PWE has been effectively applied not only to index guiding PCFs but also to PBGFs. PWE involves defining the supercell over a restricted region and using periodic boundary conditions to extend the structure spatially, and therefore, the applicability to PCFs that do not need to be periodic is somewhat restricted. An alternative approach is a localized-function method (LFM). As the guided modes in PCFs are localized in the defect core region, their modal fields are well described using localized Hermite-Gaussian functions. The LFM takes advantage of mode localization, and thus, a modest number of functions are required to accurately model the guided modes, resulting in less computational efforts, compared with the PWE.

### 2.1.3 Numerical approach

Although the basis-function expansion approach can accurately predict the modal properties such as dispersion and birefringence, it is difficult to apply it to more complicated fibers with noncircular air holes and/or longitudinally varying structures. Recently, published models utilize other direct numerical analysis techniques such as BPM, FDM, FDTD, BEM, and FEM. In the FEM, instead of solving the wave equation, the corresponding functional to which a variational method is applied is set up, where the fiber cross section is divided into the so-called elements, an equivalent discretized model for each element is constructed, and then all the element contributions to the whole fiber cross section are assembled.

### 2.2 Full Vectored Finite Element Method

> A finite element optical mode solver is the most popular method to thoroughly analyze photonic crystal fibers. The finite element method is a numerical approximation process used for the solution of boundary and initial value problems for differential equations
> The FEM produces approximate solutions by writing them as linear combinations of simple basis functions and test functions equal to the basic functions and introducing these into the variational formulation of the problem
> The final FEM equations that must be solved are systems of linear algebraic equations
> COMSOL is modern software embedding the FEM with a cleverly designed user interface designed to increase the applicability and ease of use of mathematical modeling methods

There is different matched layer condition in finite element method.
2.2.1 Perfect Magnetic conductor: - This boundary condition can be expressed as

$$
\begin{aligned}
& n . D=0 \\
& n \times H=0
\end{aligned}
$$

According to this condition, tangential components of H and normal components of D is continuous across any interface
2.2.2 Perfect Electric conductor This boundary condition can be expressed as

$$
\begin{gathered}
n . B=0 \\
n \times E=0
\end{gathered}
$$

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Here, n is the unit normal vector to the boundary. According to this condition, tangential components of E and normal components of B is continuous across any interface.

### 2.3 Comsol Multiphysics

COMSOL MULTIPHYSICS software is used to check different properties of PCF. COMSOL software (5.1) is used for the numerical answers \& graphs of different parameters of spiral PCF and the results are reported in this thesis.

### 2.3.1 Design of PCF using COMSOL

> Open software COMSOL 5.1. A window named Model Wizard will be opened
$>$ Then following steps are followed: optics Module $>$ Wave optics $>$ Electromagnetic, frequency domain Waves $>$ Mode analysis
> The software is opened with working window.
To design the structure of a PCF first set it at appropriate modal analysis, then draw the structure of PCF and give input for geometrical properties, initialize mesh and then solve the structure. The procedure for this work is given bellow

### 2.3.1.1Setting appropriate parameter and study

$>$ We Select Physics in the Physics menu to open the Application Mode Properties dialog box.
> We select the correct study using Add study dialog box
> We select the appropriate parameter for our geometry and define all the parameter in setting window of the parameter.

### 2.3.1.2 Geometry Modeling

$>$ On geometry, toolbar click primitive and choose circle
> In setting window of circle locate size and shape
$>$ We start by drawing a circle with the radius and the center at desired values with right click in geometry icon.
> In geometry tool bar click transforms and select rotate.
> Click the build all object button.

### 2.3.1.3 Material setting

> After making the geometry of PCF we add material in our geometry.
> First, click on material toolbar and select blank material and write the refractive index of material in material setting window
> Select domain

### 2.3.1.4 Mesh setting

39
> In modal builder window $>$ component 1 click mesh 1
In setting window for mesh choose physics controlled Mesh
> From element size list select between fine to extra coarser
> Click on build all button

### 2.3.1.5 Study Setting

> In modal builder window under study $\mathbf{1}$ click mode analysis.
> In the setting window for mode, analysis locates the study setting window.
$>$ In the search for mode around a text field type refractive index of the core.
$>$ In the search for frequency around text field type frequency.
> On the home, toolbar clicks compute.

### 2.3.1.6 Post processing

51
> In modal builder window under result click 1D plot group.
> Under 1D plot group select line graph.
Plot line graph between wavelength and $n_{\text {eff }}$.
$>$ Extract spreadsheet from comsol to excel.

## CHAPTER 3

## LITERATURE SURVEY


#### Abstract

16 Md Asiful Islam and M Shah Alam proposed a structure of spiral PCF. This PCF can be used to compensate the dispersion properties and used for supercontinuum generation. The structure contains the $\frac{7}{7}$ holes in silica material. there is N circular air hole in each arm and diameter of each air hole is increased progressively. The angular displacement of each arm is $\theta$ than by previous one. the proposed structure contains an elliptical air hole at the eenter of air core This design is simulated by comsol Multiphysics which is based on full vector finite element method. The design of PCF shows the dispersion of 293.5 and $-393 \mathrm{ps} / \mathrm{nm} \mathrm{km}$. another exceptional feature of this design is their high birefringence of 0.0278 .


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Agrawal, A., Kejalakshmy, N., Rahman, B.M.A. and Gratton, K.T.V. (2009) [2] the proposed spiral PCF fiber design in the SF57 is presented with high nonlinearity with low and flattened dispersion. The design of PCF is inspired by nature Fach arm of PCF contains air holes with constant radius r and angular displacement $\theta$. A full vector finite element method is used to simulate the design. ES-PCF design in SF57 has been presented that have high nonlinearity of $2150 / \mathrm{W} / 18 \mathrm{~km}$ at 1550 nm and also the PCF optimized for low dispersion of $0.8 \mathrm{Ps} / \mathrm{nm} . \mathrm{km}$. it combines the advantage of better dispersion control with the smaller effective area and high nonlinearity.
M. Samiul Habib, M. Selim Habib, M. Imran Hasan, S.M.A Razzak (2013) [3], this paper presents a soft glass spiral photonic crystal fiber for tune two zero dispersion wavelength in the visible and near infrared region. The design contains six circular rings and eight spiral arm, each air hole of the first ring is the starting point of a spiral arm. The distance of second air ole ${ }_{69}$ the spiral arm from the center is $r_{b 1}=r_{2}+0.8\left(2 \times r_{a}\right)$ with an angular shift $\theta_{1}=\frac{360}{2 \times \mathrm{N}}$ where N is the number of spiral arms. To produce high birefringence, an artificial defect is introduced in the core region. The 2 signed fiber has two ZDW at 700 nm and 1050 mm with very large nonlinearity of $7326 / \mathrm{W} . \mathrm{Km}$ at 700 nm and $3919 / \mathrm{W} . \mathrm{Km}$ at 1050 nm . The designed PCF offer birefringence of 0.1 at $1.8 \mu \mathrm{~m}$.
S. Revathi*, Srinivasa Inabathini, Ram Sandeep (2015) [4] This paper present a soft glass spiral photonic crystal fiber with a circular air hole for achieving high birefringence, large nonlinearity, and large negative dispersion. For achieving high birefringence, the defect is introduced in the core region. The structure is designed using the comsol 3.5 it is based on finite element method, an accurate numerical method used to find the solution of boundary problems. The structure contains 8 spiral arms and each arm contains five circular air hole. An elliptical air hole introduced in the center of core with semi major axis a and semi minor axis $b$. this fiber can be used as polarization maintaining fiber which has more control on polarization. This fiber optimized for high birefringence of $2.96 \times 10^{-2}$ at $1.55 \mu \mathrm{~m}$ and high nonlinearity of $5828 / \mathrm{W} . \mathrm{Km}$.this fiber give negative dispersion $-1546.6 \mathrm{ps} / \mathrm{nm} . \mathrm{km}$ at 850 nm .
S. Revathi*, Srinivasa Inabathini and Rizwan Ali Saifudeen (2014) [5] the proposed structure is designed with elliptical air hole using comsol. The structure is designed with chalcogenide glass. This structure ${ }_{2}$ optimized for different ellipticity ratio of the air hole. The structure contains seven spiral arms and each arm contains five elliptical air holes. The angular displacement between two adjacent elliptical air hole is $\frac{180}{\mathrm{~N}}$ where N is the number of air holes in a ring. The effect of ellipticity ratio on the various property of fiber is observed. The advantage of spiral structure is low effective area and high nonlinearity. By obtaining result from simulation, we get high birefringence of order $10^{-2}$ which is larger than conventional PCF. Fiber offers high birefringence of 0.0256 at $1.55 \mu \mathrm{~m}$ and gets negative dispersion of -1136.69 at $.85 \mu \mathrm{~m}$. We can use this fiber in the nonlinear application.

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Varshali Sharma, Ritu Sharma (2016) [6] the proposed design of PCF with elliptical and circular air hole is analysed for high birefringence and large flattened dispersion. There are five rings, inner three rings have elliptical air hole and outer two rings have civcular air holes. These layouts are designed and analysed and also compare $\frac{44}{}$ ith layout having only circular air holes arrangement. From the analysis, we observed flettened dispersion over a large range from 1.2 to $1.8 \mu \mathrm{~m}$.the proposed design also give high birefringence value which can be used in various sensing application.

Philip ${ }^{70}$ St.J. Russell (2006) [7] Photonic crystal fiber with a periodic transverse microstructure have been in practical since 1996. It is now possible to manufacture PCF of a scale 10 nm on a scale of lum scale, which allows exceptional control on optical properties like dispersion, effective area, birefringence and nonlinearity of optical fiber. The novel idea for developing PCFs was the creation of a new design dielectric waveguide, one that guides light by means of a two-dimensional (2-D) PBG. the idea was to trap the light in two dimensional PCF by using air holes array.
6
Theis P. Hansen, Jes Broeng, Stig E. B. Libori, Erik Knudsen, Anders Bjarklev, Jacob Riis Jensen, and Harald Simonsen (2001) [9], photonic crystal fiber offers new possibilities of highly birefringence fiber due to large index difference between core and 6 cladding region compared to conventional fiber. The proposed design consists triangular lattice of air holes with a pitch of $4.5 \mu \mathrm{~m}$. the core is made by removing two air holes. 6
The fiber was found to exhibit the highest birefringence of $6.9 \times 10^{-4}$ at frequency $1.05 \mu \mathrm{~m}$. by optimizing the design of PCF, we get high birefringence at $1.55 \mu \mathrm{~m}$ for pitch ratio $1.7 \mu \mathrm{~m}$.
Md. Ibadul Islam, Kawsar Ahmed, Sayed Asaduzzaman, Bikash Kumar Paul a, Touhid Bhuiyan, Shuvo Sem, Md. Shadidul Islam, Sawrab Chowdhury (2017) [10], proposed structure consists air holes that are arranged in a hexagonal design of pitch $\Lambda$. The refractive index of the silica regions is 1.4445 . The holes are characterized by the area and ellipticity ratio $\frac{a}{b}$, where a and b are the diameter of the major and minor axes, respectively. Geometry of PCF is simulated for different ellipticity ratio and dole area is less than $0.4 \mu$ mit has been observed from the result that on the holes area. where ${ }_{3}$ for larger holes and ellipticities, the core itself has an elongated elliptical shape. for small hole area and small ellipticity, birefringence depends only on the ellipticity and not on area.
4
Jianfei Liao, Junqiang Sun, Mingdi Du, and Yi Qin (2014) [11], the structure consists spiral photonic crystal fiber that is used as a sensor. This design can be used to sense the colorless gas and air pollution by metering gas condensate elements. The proposed structure simulated by finite element method. Design consist of a cluster of circular air holes in core region which are formed into porous shape and cladding is formed in a
spiral shape. The proposed structure gives high sensitivity and high birefringence for the wavelength range of $1 \mu \mathrm{~m}$ to $1.8 \mu \mathrm{~m}$. we get high birefringence of $7.23 \times 10^{-3}$ at $1.33 \mu \mathrm{~m}$. so proposed spiral PCF ensure major change in colorless and toxic gas detection.

Jianfei Liao, Tianye Huang, Zuzhou Xiong, Fangguang Kuang, Yingmao Xie (2017) [12] proposed design has been analysed for large flattened dispersion and high nonlinearity coefficient. Design consist slotted core region surrounded by the three rings of air hole in the spiral lattice. The optical properties of this fiber designed has been analysed for the wavelength range from 1.4 to $1.7 \mu \mathrm{~m}$. Simulation results show that the nonlinear coefficients as high as $224.36 \mathrm{~W}^{-1} \mathrm{~m}^{-1}$ and $226.39 \mathrm{~W}^{-1} \mathrm{~m}^{-1}$ respectively. Chromatic dispersion $(-5.64,2.62)$ for wavelength range 1.4 to $1.7 \mu \mathrm{~m}$.

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Md. Ibadul Islam1, Maksuda Khatun1, Shuvo sen1, Kawsar Ahmed1 and Sayed Asaduzzaman (2016) [13] author proposed a design of spiral photonic crystal fiber having an elliptical slot in core region for purpose of controlling dispersion and birefringence property of PCF. Elliptical slot in the core region is made of SF57 (soft glass). fiber cladding consists of spiral lattice on fused silica having refractive index 1.45. the diameter of air hole in each arm is increase respectively. Here SF57 is used for two regions 1) SF57 has high nonlinearity. 2) it enhances the confinement of light in high index SF57 area.in addition of this SF57 also alter the chromatic dispersion and destroy the symmetry of fiber and increase birefringence.by examining the design, the result shows birefringence of 0.0341 at $1.55 \mu \mathrm{~m}$.dispersion at 1.55 is $-491.16 \mathrm{ps} / \mathrm{nm}-\mathrm{km}$.

Jianfei Liao Yingmao Xie Xinghua Wang Dongbo Li Tianye Huang(2017) [14], the proposed design of spiral PCF has been used in gas sensing application. Inner core region consists hexagonal lattice and shape of air holes is elliptical. Outer cladding region having spiral lattice. In fiber design, there is 10 spiral arms and each arm has 9 circular air holes. It has been observed from a simulation that relative sensitivity is $42.27 \%$ and due to the presence of hexagonal lattice in the core region, we observe high birefringence of order ( 0.01727 ) at $1.33 \mu \mathrm{~m}$ wavelength range.

Arti Agrawal, Y. O. Azabi and B. M. A. Rahman (2013) [15] the proposed structure contains slotted silicon PCF with ultra-high birefringence, nonlinearity, and ultrahigh flattened dispersion. Cladding consists of a triangular lattice of air holes of diameter D and pitch $\Lambda$.in addition of this a design consists elliptical silicon nichrome rod, is situated in the center of the core that breaks the symmetry of design and increases birefringence of fiber. Simulation result shows that by introducing silicon nichrome rod birefringence of order 0.0736 at $1.55 \mu \mathrm{~m}$ is achieved. Low dispersion of $.49 \mathrm{ps} / \mathrm{nm}-\mathrm{km}$ is achieved at 180 nm . The designed PCF can be used as power efficient optical application.
${ }_{50}{ }_{50}$ Stu Sharma, Vijay Janyani, S. K. Bhatnagar (2011) [16], index core two-dimensional 50 photonic crystal fiber has been proposed in this paper modal analysis is done by FDTD for TE and TM mode. The PCF consist three rings of elliptical air and compare with circular air hole design.by observing the result of simulating designs we analyse that elliptical air hole design gives lower dispersion as compared to circular air hole design.

Rui Hao, Guifang Sun (2015) [17], An elliptical spiral soft glass PCF has been designed and analysed for high birefringence. The geometry is inspired by nature, such as galaxies, distribution of sunflower, shells of snails etc. PCF consist 12 circular air hole and spiral lattice having same ellipticity ratio from the first ring to the last ring. Due to the compactness of design light confinement in PCF is tight than conventional fiber. By examined the simulation result, for wavelength range $1000-1800 \mathrm{~nm}$, designed PCF offer birefringence up to 0.05554 .

## CHAPTER 4

## NUMERICAL ANALYSIS OF SPIRAL PCF

### 4.1 Introduction

In this chapter, two dimensional spiral PCF has been designed using Comsol 5.1. Comsol 5.1 is based on finite element method. [1-5] The Design contains of five rings of circular air holes in the spiral lattice. Three configurations of spiral PCF have been analysed for different optical properties such as effective refractive index, dispersion, effective area etc. In these three configurations, the diameter of air hole is changed and all another parameter like pitch etc. is kept constant. Approaching from circular air hole spiral PCF to elliptical air hole spiral PCF air filling fraction is kept same and the results are compared. [20-21]

### 4.2 Design Parameter of Circular spiral PCF

| NAME | VALUE | DISCRIPTION |
| :---: | :--- | :--- |
| d | $1,0.8,0.8[\mu \mathrm{~m}]$ | Diameter of air hole <br> 15 |
| $\mathrm{r}_{0}$ | $2[\mu \mathrm{~m}]$ | Radius of first air hole |
| $\mathrm{r}_{1}$ | $3.8[\mu \mathrm{~m}]$ | Radius of second air <br> hole <br> 15 |
| $\mathrm{r}_{2}$ | $5.6[\mu \mathrm{~m}]$ | Radius of third air hole |
| $\mathrm{r}_{3}$ | $7.4[\mu \mathrm{~m}]$ | Radius of fourth air hole |
| $\mathrm{r}_{4}$ | $9.2[\mu \mathrm{~m}]$ | Radius of fifth air hole |
| W | $1.55[\mu \mathrm{~m}]$ | wavelength |
| f | C const $/ \mathrm{w}$ | frequency |
| $\mathrm{n}_{\text {core }}$ | 1.45 | Refractive index |
| $\mathrm{n}_{\text {air hole }}$ | 1 | Refractive index |

### 4.3Geometry of Circular air hole spiral PCF



38
Figure 4.1 Snap shot of Circular air hole spiral PCF with (a) $\mathrm{d}=0.6[\mu \mathrm{~m}]$ (b) $\mathrm{d}=0.8[\mu \mathrm{~m}]$

$$
\text { and }(\mathrm{c}) \mathrm{d}=1[\mu \mathrm{~m}]
$$

### 4.4 Snapshot of mode profile



Fig:4.2 (a) $\mathrm{d}=1[\mu \mathrm{~m}]$


Fig:4.2 (b) $\mathrm{d}=0.8[\mu \mathrm{~m}]$


Fig:4.2 (c) $\mathrm{d}=0.6[\mu \mathrm{~m}]$

Mode profile of Spiral PCF is shown at $1.55 \mu \mathrm{~m}$ wavelength for the fundamental mode. Color variation (red for maximum, blue for minimum power) for power is shown. From this figure, it is shown that maximum light is passed through the core, not in the cladding.

## 58 <br> 4.5 Effective mode index

COMPARISION OF REFRACTIVE INDEX


Figure 4.3 refractive index vs wavelength plot for $\mathrm{d}=1,0.8,0.6[\mu \mathrm{~m}]$
3
Fig 4.3 shows the 49 riation of effective index with wavelength for different circular air hole spiral PCF. It can be analysed that the slope of Effective refractive index increases with a diameter of air holes. Relation between $n_{e f f}$ and wavelength is given as

$$
\beta=\frac{2 \pi}{\lambda} \times n_{e f f}
$$

From above formula, there is reciprocal relation between $n_{\text {eff }}$ and wavelength and it is verified from the Fig 4.3.

### 4.6 Dispersion profile

Total dispersion is the variation of group velocity with variation in wavelength. Dispersion of PCF is highly effected by the size of air holes and the air hole arrangement in geometry. Another parameter that can alter dispersion profile is a number of spiral arm and size of the core. From Fig 4.4, it can be analysed that dispersion is minimum for diameter $0.6 \mu \mathrm{~m}$ and maximum for diameter $1 \mu \mathrm{~m}$. Total dispersion (chromatic dispersion) made of two form of component (1) waveguide dispersion (2) material dispersion [28]


5
Fig 4.4 Plot of waveguide dispersion ( $\mathrm{ps} / \mathrm{nm}-\mathrm{km}$ ) $\mathrm{v} / \mathrm{s}$ wavelength for $\mathrm{d}=1[\mu \mathrm{~m}], 0.8$

$$
[\mu \mathrm{m}] \cdot 0.6[\mu \mathrm{~m}] .
$$

### 4.7 Effective ${ }_{4}$ rea

In Figure 4.5, the effect of diameter of air hole on the effective area is analysed. Effective area linearly increases with wavelength. The effective area of conventional PCF is high over a spiral photonic crystal fiber. This less effective area is an advantage over conventional PCF. Due to the less effective area, this fiber can be used in the nonlinear application. It can be observed from Fig 4.5 that as we increase the diameter of the air hole effective area get reduced and at diameter $1 \mu \mathrm{~m}$ we get low effective area than others. [11]


17
Fig:4.5 Plot of Effective Area vs wavelength for $\mathrm{d}=1[\mu \mathrm{~m}], 0.8[\mu \mathrm{~m}], 0.6[\mu \mathrm{~m}]$.

### 4.8 Design Parameters of Elliptical Air hole spiral PCF

| NAME | VALUE | DISCRIPTION |
| :---: | :--- | :--- |
|  |  |  |
| d | $1[\mu \mathrm{~m}]$ | Diameter of air hole <br> 15 |
| $\mathrm{r}_{0}$ | $2[\mu \mathrm{~m}]$ | Radius of first air hole |
| $\mathrm{r}_{1}$ | $3.8[\mu \mathrm{~m}]$ | Radius of second air hole <br> 15 |
| $\mathrm{r}_{2}$ | $5.6[\mu \mathrm{~m}]$ | Radius of third air hole |

### 4.9 Geometry of elliptical air hole spiral PCF



Figure 4.6 snap shot of elliptical air hole spiral PCF a: major axis b: minor axis of ellipse Fig 4.6(a) $\mathrm{a}=.0 .57[\mu \mathrm{~m}], \mathrm{b}=0.43[\mu \mathrm{~m}]$ Fig 4.6(b) with different ellipticity Fig 4.6(c)

$$
\mathrm{a}=0.62[\mu \mathrm{~m}], \mathrm{b}=0.40
$$

### 4.10 Snapshot of mode profile



Figure 4.7 Snap shot of mode profile for different Elliptical air hole spiral PCF
Fig 4.7(a) $\mathrm{a}=0.57[\mu \mathrm{~m}], \mathrm{b}=0.43[\mu \mathrm{~m}]$ Fig 4.7 (b) with different ellipticity Fig 4.7(c)

$$
\mathrm{a}=0.62[\mu \mathrm{~m}], \mathrm{b}=0.40
$$

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In given figure, red color shows the maximum intensity of light and blue color shows the 57 mimum intensity of light. From mode profile, we can examine that most of the light is confined in core region due to refractive index variation. Confinement in PCF is high than conventional fiber. This is the advantage of PCF over conventional fiber.[24]

### 4.11 Refractive index vs wavelength

The wavelength is varied from $0.2 \mu \mathrm{~m}$ to $2 \mu \mathrm{~m}$ for the simulation. $\mathrm{n}_{\text {eff }}$ is calculated by simulating the design. The variation in effective refractive index $\mathrm{v} / \mathrm{s}$ wavelength is shown in Fig 4.8. It can be examined from the graph that effective refractive index decreases as the wavelength is increased. From the graph, it observed that the slope of effective refractive index increases with ellipticity ratio.


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Figure 4.8(a) Plot of Effective refractive index $\mathrm{v} / \mathrm{s}$ wavelength for ellipticity ratio
1.22,1.32,1.55.


Fig 4.8(b) zoom view of refractive index vs wavelength plot


Fig 4.9(a) Plot of Total dispersion $\mathrm{v} / \mathrm{s}$ wavelength for ellipticity ratio $1,1.22,1.32,1.64$


Fig 4.9(b) Plot showing Flat range of dispersion $v / s$ wavelength

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It can be analysed that dispersion is highly affected by the size of air hole so if the air filling fraction is increased or size of air hole is increased the dispersion also changes.

From Fig 4.8 and Fig 4.9, it can be analysed that for ellipticity ratio 1.64 we get the highest dispersion and for graded size air hole we get minimum distortion.So if ellipticity ratio from the first ring to the last ring is increased or decreased the magnitude of dispersion is highly affected. A minimum magnitude of dispersion is obtained for ellipticity ratio 1.22 . From figure 4.9 (b) it can be examined that nearly flat dispersion is pbtained from $1.5 \mu \mathrm{~m}$ to $1.68 \mu \mathrm{~m}$ wavelength range. An important fact that can be observed from the Fig 4.9 is that when the geometry is changed from circular to elliptical air holes, the magnitude of dispersion gets increased but birefringence also increases.[21]

### 4.13 Birefringence

Birefringence is the difference between the two orthogonal directions. Modal birefringence is defined as [12]

Birefringence $=\left[\mathrm{n}_{\text {eff }}(\mathrm{X}\right.$ mode $)-\mathrm{n}_{\text {eff }}(\mathrm{Y}$ mode $\left.)\right]$


Fig 4.10(a) snap shot of $X$ polarization

Fig 4.10 (a) snap shot of X polarization mode


Fig 4.10(b) snap shot of $Y$ polarization

Fig 4.10 (b) snap shot of $Y$ polarization mode

### 4.14 Birefringence v/s Ellipticity ratio



Fig 4.11 Plot of ellipticity ratio vs wavelength
24
The effect of ellipticity ratio on wavelength is shown in Fig 4.11. It can see from the graph that birefringence varies with ellipticity ratio. In the plot, the ellipticity range is varied from 0.8 to 2.4 and for ellipticity ratio 2.2 , we get the highest value of birefringence.

### 4.15 Birefringence $\mathbf{v} / \mathrm{s}$ Wavelength

The proposed PCF consists of an elliptical-Spiral arrangement of the air hole. In comparison to conventional PCF structure supporting different properties, the compact design of elliptical air hole spiral PCF achieves large birefringence. From Figure 4.12, it can be seen that birefringence increases linearly with frequency [26]. We get high birefringence for ellipticity ratio 1.64 for wavelength range 1.50 to $1.80 \mu \mathrm{~m}$, designed PCF offered high birefringence up to 0.004 .


Fig 4.12 Plot of Birefringence $\mathrm{v} / \mathrm{s}$ wavelength for different ellipticity ratio

### 4.16 Effecti ${ }_{26}$ area $\mathrm{v} / \mathrm{s}$ wavelength plot

From the plot shown in Fig 4.13, the effect of ellipticity ratio on the effective area can 19 examined. It is observed that effective area of elliptical air hole spiral PCF linearly increases with wavelength. The effective area of elliptical air hole spiral PCF is considerably small than conventional fiber. This property of PCF can be used in various nonlinearity application such as supercontinuum generation, four waves mixing etc. It can be observed from the plot that at ellipticity ratio 1.55 , the effective area is lowest as compared others.


Fig 4.13(a) Effective area $\mathrm{v} / \mathrm{s}$ wavelength plot


Fig 4.13 (b) zoom view of Effective area $\mathrm{v} / \mathrm{s}$ wavelength p

## CHAPTER 5

## COMPARATIVE STUDY AND CONCLUSION

### 5.1 Introduction

This chapter deals with the comparative analysis of different characterstics of spiral photonic crystal fiber like effective mode index, waveguide dispersion and chromatic dispersion by varying wavelength for different diameter of air hole spiral photonic crystal fiber.[15]

### 5.2 Comparison of Effective mode index

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Fig 4.19 shows the comparative study of effective mode index. In Fig 4.19 it can be seen that as the wavelength is increased the value of $n_{\text {eff }}$ decreases. Fig 4.19 shows that the slope of refractive index $\mathrm{v} / \mathrm{s}$ wavelength plot is maximum for elliptical air hole spiral PCF as compared with circular air hole PCF.

Table 5.1 Wavelength $\mathbf{v} / \mathrm{s}$ effective refractive index

| wavelength | $\mathrm{a} / \mathrm{b}=1.22$ | $\mathrm{a} / \mathrm{b}$ <br> $=1.32$ | $\mathrm{a} / \mathrm{b}=1.55$ | $\mathrm{a} / \mathrm{b}=$ graded | neff <br> $\mathrm{d}=1[\mathrm{um}]$ | neff <br> $\mathrm{d}=.8[\mathrm{um}]$ | neff <br> $\mathrm{d}=.6[\mathrm{um}]$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.2 | 1.449166853 | 1.449151 | 1.449173039 | 1.449151355 | 1.449721812 | 1.449743592 | 1.449784087 |
| 0.305882353 | 1.448092071 | 1.448057 | 1.448105572 | 1.448056659 | 1.449360212 | 1.449412177 | 1.449506576 |
| 0.411764706 | 1.446612718 | 1.44655 | 1.446635343 | 1.446550049 | 1.448860308 | 1.448956318 | 1.449127117 |
| 0.517647059 | 1.444752092 | 1.444656 | 1.444785287 | 1.444656022 | 1.448229799 | 1.448384668 | 1.448654858 |
| 0.623529412 | 1.442532128 | 1.442398 | 1.442577074 | 1.442397615 | 1.447476559 | 1.447706235 | 1.448099731 |
| 0.729411765 | 1.439734601 | 1.439578 | 1.440031218 | 1.439796464 | 1.446608729 | 1.446930514 | 1.447472466 |
| 0.835294118 | 1.436747866 | 1.43656 | 1.437167239 | 1.436872939 | 1.445634794 | 1.446067536 | 1.446784355 |
| 0.941176471 | 1.433437125 | 1.43322 | 1.433453364 | 1.433646334 | 1.444563643 | 1.445127821 | 1.446046878 |
| 1.047058824 | 1.429820031 | 1.429578 | 1.429821449 | 1.4301351 | 1.443404583 | 1.444122218 | 1.44527127 |
| 1.152941176 | 1.425914275 | 1.425652 | 1.42589325 | 1.426357078 | 1.442167287 | 1.44306169 | 1.444468127 |
| 1.258823529 | 1.421737785 | 1.421462 | 1.421685639 | 1.422329697 | 1.4408617 | 1.441957056 | 1.443647091 |
| 1.364705882 | 1.417308825 | 1.417026 | 1.41721593 | 1.41807006 | 1.439497899 | 1.440818747 | 1.442816623 |
| 1.470588235 | 1.412645929 | 1.412365 | 1.412501872 | 1.413594847 | 1.438085938 | 1.439656573 | 1.441983883 |
| 1.576470588 | 1.40776757 | 1.407497 | 1.407561426 | 1.408919975 | 1.436635675 | 1.438479534 | 1.441154705 |


| 1.682352941 | 1.402691513 | 1.402442 | 1.402412262 | 1.404059973 | 1.435156604 | 1.437295687 | 1.440333644 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.788235294 | 1.397433823 | 1.397214 | 1.397070941 | 1.399027094 | 1.433657705 | 1.436112051 | 1.439524076 |
| 1.894117647 | 1.392007662 | 1.391827 | 1.391551818 | 1.393830249 | 1.432147303 | 1.434934579 | 1.438728337 |



Fig 5.1(a) comparision of $n_{\text {eff }} \mathrm{v} / \mathrm{s}$ wavelength for diameter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$


Fig 5.1(b) Zoom View of Fig 5.1(a)

## 5.3 comparision of waveguide dispersion

Fig 5.20 shows a variation of dispersion with wavelength and it can be seen from the graph that as we increase the diameter of airhole dispersion also increases.


Fig 5.2 waveguide dispersion $\mathrm{v} / \mathrm{s}$ wavelength for dimeter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$

## 5.4 comparision of chromatic dispersion(total dispersion) <br> Table 5.2 Wavelength v/s total dispersion

| wavelength | $a / b=1.32$ | $\mathrm{a} / \mathrm{b}=1.22$ | $a / b=1.64$ | mix | $\mathrm{a} / \mathrm{b}=1.0 \mathrm{um}$ <br> circular | $\mathrm{d}=0.6 \mathrm{um}$ | $\mathrm{D}=0.8 \mathrm{um}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.517647059 | $631.8940409$ | $631.8957836$ | -641.136751 | -640.304876 | $677.5611786$ | $683.7168533$ | -680.024165 |
| 0.623529412 | $245.4728624$ | $246.3333746$ | -261.64019 | -260.833925 | $303.2061562$ | $311.0864995$ | -306.422742 |
| 0.729411765 | $104.0996341$ | $104.1374419$ | -104.299298 | -103.525587 | $150.5085352$ | -160.312355 | -154.600807 |
| 0.835294118 | $34.54773613$ | $34.51025927$ | 16.39738005 | -30.2269825 | $81.43242087$ | $93.27491991$ | -86.5129079 |
| 0.941176471 | 22.76285561 | 21.73327127 | 85.41220659 | 16.72897307 | $38.38854081$ | $52.24782281$ | -44.5331464 |
| 1.047058824 | 50.93237015 | 49.38628283 | 86.46978143 | 44.17308078 | $14.57959505$ | $30.26835016$ | -21.8043405 |
| 1.152941176 | 75.63847525 | 73.52690224 | 90.89383425 | 68.36791401 | 6.258813238 | $10.90495025$ | -1.98725523 |
| 1.258823529 | 94.46920131 | 91.75597403 | 99.21576505 | 86.96833067 | 21.79047736 | 3.65205423 | 12.66207736 |


| 1.364705882 | 105.0723451 | 101.7400514 | 110.5827549 | 97.69374364 | 29.70546452 | 11.20029635 | 19.90978681 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1.470588235 | 116.1491334 | 112.2145752 | 122.3159461 | 109.3133502 | 38.64923401 | 20.44435016 | 28.46475035 |
| 1.576470588 | 116.3013997 | 111.8417734 | 122.8905755 | 110.4779158 | 36.99938551 | 19.76981603 | 26.74891725 |
| 1.682352941 | 116.2271908 | 111.4052306 | 122.8489322 | 111.9023659 | 35.01027064 | 19.3916755 | 25.03795682 |
| 1.788235294 | 116.6914955 | 111.7601394 | 122.8176309 | 114.3325155 | 32.80046206 | 19.35024654 | 23.44774087 |
| 1.894117647 | 133.2507909 | 128.3315139 | 138.7569288 | 132.6238378 | 45.5178704 | 33.83913783 | 36.69932799 |



Fig 5.3 comparision of chromatic dispersion $\mathrm{v} / \mathrm{s}$ wavelength
Chromatic dispersion is a combination of two type of dispersio ${ }_{37}{ }^{1}$ ) waveguide dispersion 2) material disersion. Dispersion in PCF is highly effected by the size of air holes and arrangement of air hole in cladding region. The dispersion propery can be altered by chaming the geometry of PCF. Fig 5.3 shows the variation of dispersion with wavelength, it can be observed from the Fig 5.3 that the magnitude of dispersion is minimum for circular air hole spiral PCF and higher for eliptical air hole spiral PCF. At $1.55 \mu \mathrm{~m}$, the minimum dispersion obtained for $0.6 \mu \mathrm{~m}$ circular air hole. By comparing the result of circular air hole spiral PCF for diameter $1 \mu \mathrm{~m}$ and elliptical air hole spiral PCF for same air filling fraction, we get lower dispersion for circular air hole spiral PCF.

### 5.5 Comparison of zero dispersion wavelength

## Table 5.3 Zero dispersion wavelength

| Circular air hole | Zero dispersion <br> wavelength | Elliptical air hole | Zero dispersion <br> wavelength |
| :--- | :--- | :--- | :--- |
| Diameter $=1.0$ <br> $[\mu \mathrm{~m}]$ | $1.12[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.22$ | $0.901[\mu \mathrm{~m}]$ |
| Diameter $=0.8$ <br> $[\mu \mathrm{~m}]$ | $1.18[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.32$ | $0.896[\mu \mathrm{~m}]$ |
| Diameter $=0.6$ <br> $[\mu \mathrm{~m}]$ | $1.24[\mu \mathrm{~m}]$ | Ellipticity ratio $=1.62$ | $0.835[\mu \mathrm{~m}]$ |
|  |  | Ellipticity <br> ratio= graded | $0.903[\mu \mathrm{~m}]$ |



Fig 5.4(a) zero dispersion wavelength at diameter $=1 \mu \mathrm{~m}, 0.8 \mu \mathrm{~m}, 0.6 \mu \mathrm{~m}$


Fig 5.4(b) zoom view of above graph
5
the zero-dispersion wavelength is the wavelength at whieh waveguide dispersion and material dispersion and cancel one another. In fig 5.4(a) it can be seen that as we reduce the diameter of air hole zero dispersion wavelength shift toward right hand side. By analyzing the result of both designs, it observe that as we change the geometry of air holes from circular to elliptical, zero dispersion wavelength get shifted to the lower side of wavelength. [23]

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### 5.6 Comparison of effective area

Table 5.3 Wavelength v/s effective area

| w [ $\mu \mathrm{m}$ ] | $a / b=1.22$ | $a / b=1.32$ | $a / b=1.55$ | graded | $\mathrm{d}=1 \mathrm{um} \mathrm{c}$ | $\mathrm{d}=0.8 \mathrm{um}$ <br> c | d=0.6 c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.2 | 3.77213 <br> 1186 | 3.78641 <br> 5948 | $\begin{aligned} & 3.76221 \\ & 508 \end{aligned}$ | $\begin{aligned} & 3.89639 \\ & 6857 \end{aligned}$ | $\begin{aligned} & 3.82307 \\ & 1697 \end{aligned}$ | 4.42673 <br> 5403 | $\begin{aligned} & 5.14322 \\ & 8341 \end{aligned}$ |
| 0.30588 2353 | $\begin{aligned} & 3.84969 \\ & 0648 \end{aligned}$ | $\begin{aligned} & 3.86429 \\ & 3064 \end{aligned}$ | $\begin{aligned} & 3.83991 \\ & 9906 \end{aligned}$ | $\begin{aligned} & 3.97183 \\ & 1001 \end{aligned}$ | $\begin{aligned} & 3.89276 \\ & 7746 \end{aligned}$ | 4.50645 <br> 0938 | $\begin{aligned} & 5.25345 \\ & 5655 \end{aligned}$ |
| $0.41176$ <br> 4706 | $\begin{aligned} & 3.92790 \\ & 0397 \end{aligned}$ | $3.94271$ | $3.91775$ <br> 6542 | $\begin{aligned} & 4.04791 \\ & 7293 \end{aligned}$ | 3.96340 <br> 9882 | 4.58807 <br> 1714 | 5.37541 498 |
| $\begin{aligned} & 0.51764 \\ & 7059 \end{aligned}$ | $\begin{aligned} & 4.00734 \\ & 6111 \end{aligned}$ | 4.02214 <br> 8574 | 3.99638 <br> 1016 | 4.12457 <br> 6639 | 4.03518 <br> 0071 | $\begin{aligned} & 4.67239 \\ & 4294 \end{aligned}$ | 5.51534 <br> 3806 |


| $\begin{aligned} & 0.62352 \\ & 9412 \end{aligned}$ | $\begin{aligned} & 4.08922 \\ & 9882 \end{aligned}$ | $\begin{aligned} & 4.10389 \\ & 3848 \end{aligned}$ | $\begin{aligned} & 4.07663 \\ & 0939 \end{aligned}$ | $\begin{aligned} & 4.20235 \\ & 9198 \end{aligned}$ | $\begin{aligned} & 4.10855 \\ & 3734 \end{aligned}$ | $\begin{aligned} & 4.76043 \\ & 7539 \end{aligned}$ | $\begin{aligned} & \hline 5.68245 \\ & 269 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 0.72941 \\ & 1765 \end{aligned}$ | $\begin{aligned} & 4.11849 \\ & 8296 \end{aligned}$ | $\begin{aligned} & 4.19000 \\ & 1386 \end{aligned}$ | $\begin{aligned} & 4.15983 \\ & 2827 \end{aligned}$ | $\begin{aligned} & 4.28206 \\ & 7549 \end{aligned}$ | $\begin{array}{\|l} 4.18377 \\ 514 \end{array}$ | $\begin{aligned} & 4.85359 \\ & 7558 \end{aligned}$ | 5.89002 2937 |
| 0.83529 4118 | 4.19897 <br> 0615 | $\begin{aligned} & 4.20942 \\ & 438 \end{aligned}$ | $\begin{aligned} & 4.24906 \\ & 3148 \end{aligned}$ | $\begin{aligned} & 4.36532 \\ & 8268 \end{aligned}$ | $\begin{aligned} & 4.26114 \\ & 6999 \end{aligned}$ | $\begin{aligned} & 4.95402 \\ & 3671 \end{aligned}$ | 6.15614 4673 |
| $0.94117$ <br> 6471 | 4.28626 <br> 6404 | $\begin{aligned} & 4.29653 \\ & 8583 \end{aligned}$ | $\begin{aligned} & 4.25032 \\ & 8471 \end{aligned}$ | $\begin{aligned} & 4.45615 \\ & 9114 \end{aligned}$ | $\begin{array}{\|l\|} \hline 4.34110 \\ 3581 \end{array}$ | $\begin{aligned} & 5.06505 \\ & 3793 \end{aligned}$ | 6.50405 <br> 4728 |
| 1.04705 <br> 8824 | 4.38350 3932 | $\begin{aligned} & 4.39408 \\ & 7191 \end{aligned}$ | $\begin{aligned} & 4.34403 \\ & 6914 \end{aligned}$ | $\begin{aligned} & 4.56428 \\ & 1211 \end{aligned}$ | $\begin{aligned} & 4.42428 \\ & 7177 \end{aligned}$ | $\begin{aligned} & 5.19168 \\ & 4424 \end{aligned}$ | 6.96196 <br> 707 |
| $1.15294$ $1176$ | 4.49535 <br> 4449 | $\begin{aligned} & 4.50690 \\ & 4522 \end{aligned}$ | $\begin{aligned} & 4.45157 \\ & 8296 \end{aligned}$ | $\begin{aligned} & 4.71069 \\ & 5973 \end{aligned}$ | $\begin{aligned} & 4.51168 \\ & 719 \end{aligned}$ | $\begin{aligned} & 5.34103 \\ & 4793 \end{aligned}$ | 7.56225 <br> 5223 |
| 1.25882 3529 | 4.62853 <br> 2812 | $\begin{aligned} & 4.64188 \\ & 9572 \end{aligned}$ | $\begin{aligned} & 4.57920 \\ & 1431 \end{aligned}$ | $\begin{aligned} & 4.93502 \\ & 3101 \end{aligned}$ | $\begin{aligned} & 4.60482 \\ & 817 \end{aligned}$ | $\begin{aligned} & 5.52275 \\ & 0946 \end{aligned}$ | 8.33983 <br> 6175 |
| 1.36470 <br> 5882 | 4.79246 <br> 0576 | $\begin{aligned} & 4.80871 \\ & 8265 \end{aligned}$ | $\begin{aligned} & 4.73559 \\ & 6964 \end{aligned}$ | $\begin{aligned} & 5.30575 \\ & 9001 \end{aligned}$ | $\begin{aligned} & 4.70600 \\ & 2609 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.74929 \\ & 0284 \end{aligned}$ | 9.32966 <br> 4759 |
| 1.47058 <br> 8235 | 5.00025 <br> 413 | $\begin{aligned} & 5.02088 \\ & 2095 \end{aligned}$ | $\begin{aligned} & 4.93277 \\ & 2544 \end{aligned}$ | $\begin{aligned} & 5.94694 \\ & 723 \end{aligned}$ | $\begin{aligned} & 4.81854 \\ & 1391 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.03603 \\ & 0659 \end{aligned}$ | $10.5634$ $1686$ |
| $1.57647$ | 5.27017 3552 | $\begin{aligned} & 5.29714 \\ & 2956 \end{aligned}$ | $\begin{aligned} & 5.18724 \\ & 9215 \end{aligned}$ | $\begin{aligned} & 7.13682 \\ & 0457 \end{aligned}$ | $\begin{aligned} & 4.94710 \\ & 728 \end{aligned}$ | $\begin{aligned} & 6.40116 \\ & 3022 \end{aligned}$ | 12.0657 <br> 5651 |
| 1.68235 <br> 2941 | 5.62758 <br> 8888 | $\begin{aligned} & 5.66344 \\ & 3122 \end{aligned}$ | $\begin{aligned} & 5.52163 \\ & 4868 \end{aligned}$ | $\begin{aligned} & 8.75949 \\ & 7803 \end{aligned}$ | $\begin{aligned} & \hline 5.09798 \\ & 7091 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.86534 \\ & 5171 \end{aligned}$ | 13.8508 8964 |
| $\begin{aligned} & 1.78823 \\ & 5294 \end{aligned}$ | $6.10742$ <br> 3164 | $\begin{aligned} & \hline 6.15522 \\ & 2861 \\ & \hline \end{aligned}$ | $\begin{aligned} & 5.96656 \\ & 4693 \end{aligned}$ | $\begin{aligned} & 10.5745 \\ & 7026 \end{aligned}$ | $\begin{aligned} & \hline 5.27934 \\ & 7959 \\ & \hline \end{aligned}$ | $\begin{aligned} & 7.45107 \\ & 4732 \end{aligned}$ | 14.9262 2588 |
| $\begin{aligned} & 1.89411 \\ & 7647 \end{aligned}$ | $\begin{aligned} & 6.75682 \\ & 8862 \end{aligned}$ | $\begin{aligned} & 6.81984 \\ & 9249 \end{aligned}$ | $\begin{aligned} & 6.56280 \\ & 3146 \end{aligned}$ | $\begin{aligned} & 12.5865 \\ & 1604 \end{aligned}$ | $\begin{aligned} & 5.50141 \\ & 6427 \end{aligned}$ | $\begin{aligned} & 8.18175 \\ & 6249 \end{aligned}$ | $\begin{aligned} & 14.9987 \\ & 1432 \end{aligned}$ |



Figure 5.5 comparison of Effective area vs wavelength plot
13
In Fig 5.5, the effect of diameter of air hole and geometry of air hole on the effective area is examined. The effective area of PCF is much smaller than conventional PCF. By analyzing the result of PCF, it is observed that elliptical air hole PCF offers high effective area than circular air hole PCF. For circular air hole PCF of diameter $1 \mu \mathrm{~m}$, a minimum effective area is obtained.

### 5.7 Birefringence vs Wavelength

. High birefringence fiber can be used as a sensor. To increase the birefringence, elliptical air holes are introduced in PCF or the symmetry of PCF is broken. It can be seen from Fig 5.6 that birefringence varies with ellipticity ratio. Because if, there is a change in ellipticity ratio air filling fraction get changed. It can be seen from the graph that for circular air hole minimum birefringence of the order $10^{-3}$ is observed and as the ellipticity ratio is increased, the magnitude of birefringence for PCF also increases.

Table 5.4 Wavelength $\mathbf{v} / \mathrm{s}$ birefringence

| Waveleng th | $a / b=1.22$ | $a / b=1.32$ | $a / b=1.55$ | $a / b=1.64$ | graded ellip holes | circular air hole |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.2 | $\begin{aligned} & 1.74847 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 1.50167 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 2.80366 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 3.14214 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 4.19246 \mathrm{E}- \\ & 06 \end{aligned}$ | $\begin{aligned} & 4.19467 \mathrm{E}- \\ & 06 \end{aligned}$ |
| $\begin{aligned} & 0.3058823 \\ & 53 \end{aligned}$ | $\begin{aligned} & 1.48852 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.46567 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.77249 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.85311 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.78522 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 1.78587 \mathrm{E}- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.4117647 \\ & 06 \end{aligned}$ | $4.26633 \mathrm{E}-$ <br> 05 | $4.29268 \mathrm{E}-$ <br> 05 | $\begin{aligned} & 4.84759 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 5.0027 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.39874 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 4.39995 \mathrm{E}- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.5176470 \\ & 59 \end{aligned}$ | $\begin{aligned} & 8.78263 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 8.92817 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 9.85487 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 0.0001013 \\ & 6 \end{aligned}$ | $\begin{aligned} & 8.50137 \mathrm{E}- \\ & 05 \end{aligned}$ | $\begin{aligned} & 8.50318 \mathrm{E}- \\ & 05 \end{aligned}$ |
| $\begin{aligned} & 0.6235294 \\ & 12 \end{aligned}$ | $\begin{aligned} & 0.0001526 \\ & 41 \end{aligned}$ | $\begin{aligned} & 0.0001562 \\ & 27 \end{aligned}$ | $\begin{aligned} & 0.0001711 \\ & 26 \end{aligned}$ | $\begin{aligned} & 0.0001759 \\ & 51 \end{aligned}$ | $\begin{aligned} & 0.0001427 \\ & 72 \end{aligned}$ | $\begin{aligned} & 0.0001427 \\ & 97 \end{aligned}$ |
| $\begin{aligned} & 0.7294117 \\ & 65 \end{aligned}$ | $\begin{aligned} & 0.0002389 \\ & 6 \end{aligned}$ | $\begin{aligned} & 0.0002458 \\ & 88 \end{aligned}$ | $\begin{aligned} & 0.0002690 \\ & 52 \end{aligned}$ | $\begin{aligned} & 0.0002768 \\ & 75 \end{aligned}$ | $\begin{aligned} & 0.0002184 \\ & 91 \end{aligned}$ | $\begin{aligned} & 0.0002185 \\ & 21 \end{aligned}$ |
| $\begin{aligned} & 0.8352941 \\ & 18 \end{aligned}$ | $\begin{aligned} & 0.0003481 \\ & 86 \end{aligned}$ | $\begin{aligned} & 0.0003599 \\ & 85 \end{aligned}$ | $\begin{aligned} & 0.0003948 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0004068 \\ & 56 \end{aligned}$ | $\begin{aligned} & 0.0003127 \\ & 74 \end{aligned}$ | $\begin{aligned} & 0.0003128 \\ & 07 \end{aligned}$ |
| $\begin{aligned} & 0.9411764 \\ & 71 \end{aligned}$ | $\begin{aligned} & 0.0004812 \\ & 57 \end{aligned}$ | $\begin{aligned} & 0.0004998 \\ & 25 \end{aligned}$ | $\begin{aligned} & 0.0005505 \\ & 49 \end{aligned}$ | $\begin{aligned} & 0.0005683 \\ & 25 \end{aligned}$ | $\begin{aligned} & 0.0004256 \\ & 15 \end{aligned}$ | $\begin{aligned} & 0.0004256 \\ & 48 \end{aligned}$ |
| $\begin{aligned} & 1.0470588 \\ & 24 \end{aligned}$ | $\begin{aligned} & 0.0006386 \\ & 42 \end{aligned}$ | $\begin{aligned} & 0.0006662 \\ & 97 \end{aligned}$ | $\begin{aligned} & 0.0007380 \\ & 86 \end{aligned}$ | $\begin{aligned} & 0.0007634 \\ & 49 \end{aligned}$ | $\begin{aligned} & 0.0005564 \\ & 16 \end{aligned}$ | $\begin{aligned} & 0.0005564 \\ & 48 \end{aligned}$ |
| $\begin{aligned} & 1.1529411 \\ & 76 \end{aligned}$ | $\begin{aligned} & 0.0008203 \\ & 19 \end{aligned}$ | $\begin{aligned} & 0.0008598 \\ & 38 \end{aligned}$ | $\begin{aligned} & 0.0009588 \\ & 7 \end{aligned}$ | $\begin{aligned} & 0.0009940 \\ & 67 \end{aligned}$ | $\begin{array}{\|l\|} \hline 0.0007040 \\ 13 \\ \hline \end{array}$ | $\begin{aligned} & 0.0007040 \\ & 39 \end{aligned}$ |
| $\begin{aligned} & 1.2588235 \\ & 29 \end{aligned}$ | $\begin{aligned} & 0.0010256 \\ & 88 \end{aligned}$ | $\begin{aligned} & 0.0010803 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0012138 \\ & 11 \end{aligned}$ | $\begin{aligned} & 0.0012615 \\ & 02 \end{aligned}$ | $\begin{aligned} & 0.0008667 \\ & 06 \end{aligned}$ | $\begin{aligned} & 0.0008666 \\ & 51 \end{aligned}$ |
| $\begin{aligned} & 1.3647058 \\ & 82 \end{aligned}$ | $\begin{aligned} & 0.0012533 \\ & 52 \end{aligned}$ | $0.0013267$ 15 | $\begin{aligned} & 0.0015029 \\ & 07 \end{aligned}$ | $\begin{aligned} & 0.0015661 \\ & 58 \end{aligned}$ | $\begin{aligned} & 0.0010422 \\ & 92 \end{aligned}$ | $\begin{aligned} & 0.0010418 \\ & 17 \end{aligned}$ |
| $\begin{aligned} & 1.4705882 \\ & 35 \end{aligned}$ | $\begin{aligned} & 0.0015006 \\ & 71 \end{aligned}$ | $\begin{aligned} & 0.0015965 \\ & 73 \end{aligned}$ | $\begin{aligned} & 0.0018244 \\ & 43 \end{aligned}$ | $\begin{aligned} & 0.0019066 \\ & 77 \end{aligned}$ | $\begin{aligned} & 0.0012281 \\ & 34 \end{aligned}$ | $\begin{aligned} & 0.0012261 \\ & 81 \end{aligned}$ |
| 1.5764705 | 0.0017629 | 0.0018847 | 0.0021733 | 0.0022782 | 0.0014213 | 0.0014151 |


| 88 | 22 | 75 | 81 | 2 | 25 | 78 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.6823529 | 0.0020319 | 0.0021818 | 0.0025389 | 0.0026698 | 0.0016190 | 0.0016024 |
| 41 | 75 | 62 | 63 | 45 | 21 | 97 |
| 1.7882352 | 0.0022953 | 0.0024735 | 0.0029046 | 0.0030644 | 0.0018189 | 0.0017793 |
| 94 | 31 | 5 | 53 | 66 | 35 | 89 |
| 1.8941176 | 0.0025385 | 0.0027456 | 0.0032560 | 0.0034475 | 0.0020198 | 0.0019346 |
| 47 | 98 | 21 | 59 | 62 | 56 | 94 |



Fig 5.6 birefringence $\mathrm{v} / \mathrm{s}$ frequency plot for different ellipticity ratio

## Conclusion and discus /47 $_{14}$

Proposed two-dimensional photonic crystal fiber has been designed and analysed for high birefringence and flattened dispersion. For analyzing the proposed design Finite Element Method has been used. The following fundamental characteristics of PCFs have been found out. They are shown in tabular format.

## Our finding

| 1.power confinement of spiral PCF for different diameter in circular spiral PCF |
| :--- |
| 2.effective mode index variation with wavelength for different diameter in circular spiral <br> PCF |
| 3.material dispersion for diffused silica at refractive index 1.45 in circular spiral PCF |
| 4.wavefuide dispersion for circular hole PCF at different diameter by varying <br> wavelength |
| 5.chromatic dispersion for circular hole PCF at different diameter by varying <br> wavelength |
| 6.zero dispersion wavelength at different diameter for circular spiral PCF |
| 7.new structure of elliptical hole spiral PCF keeping all parameter similar |
| 8.effective refractive index variation v/s wavelength for elliptical hole spiral PCF |
| 9.Chromatic dispersion vs wavelength for elliptical hole spiral PCF |
| 10.birefringence vs ellipticity ratio for elliptical hole spiral PCF |
| 11.birefringence vs wavelength plot for elliptical hole spiral PCF |
| 12.effective area vs wavelength plot for elliptical hole spiral PCF |
| 13.comparative study of different diameter circular air hole spiral photonic crystal fiber <br> and different ellipticity ratio spiral PCF |

Here we have found out properties of different diameter of air hole for doped silica spiral photonic crystal fiber. Finite 14 element method has been used for analyzing the layouts. In this report, different spiral photonic crystal fiber has been examined. By optimizing the geometry of PCF, we get almost flat dispersion in the range of $1.45[\mathrm{um}]$ to $1.70[\mathrm{um}]$. In this report, the numerically simulated result shows that a significantly lower dispersion occurs at a diameter of $0.6 \mu \mathrm{~m}$. a circular spiral PCF has been designed
in which we increase the diameter of air hole and analyzed that as we reduce the diameter of air hole dispersion also decreases and we also get the zero-dispersion wavelength shift toward right hand side as we reduce the diameter of the air hole. the designed structure also has lower dispersion than octagonal photonic crystal fiber. Due to lower dispersion, the fiber has its prominence in dispersion flatter device application. For further improvement of the result of PCF, we move from spiral circular hole to elliptical air hole spiral PCF. Due to the compactness of design, PCF offers high nonlinearity, birefringence, and low effective area. From simulation result, we observe that if we increase ellipticity ratio from 1 to 1.64 , dispersion will also increase it can be examined from the result that birefringence of order 0.003 at $1.80 \mu \mathrm{~m}$ and 0.002 at $1.55 \mu \mathrm{~m}$ is observed and Birefringence also increase with ellipticity ratio and at ellipticity ratio 1.64 , birefringence of order 0.003 is observed. From figure () is observed that effective area increases with wavelength and we get lower effective area for ellipticity ratio 1.55 .but if we compare circular air hole PCF and elliptical air hole PCF, circular air hole PCF offer lower effective area.

## Future work

Present Research work on photonic crystal fibers is based on different spiral PCF. By changing the geometry of spiral PCF and air holes ellipticity ratio, the range of flattened dispersion will be increased to significant label and birefringence will be improved. Dispersion engineering is possible in PCF in the range unachievable for classical fibers (flat dispersion in the large range, zero-dispersion, and anomalous dispersion in the visible range).

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